

ATF Report 1549

Airborne Sound Transmission
Test of a Tilt and Turn Window
with 60mm PVC frame with steel
reinforcing and 10.38mm glazing

Commissioned by
REHAU

Test Date: 10 August 2004



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 **Australian
Hearing**
National Acoustic Laboratories

ATF Report 1549

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AS1191-1985, AS1045-1988
Accredited Lab No: 5472

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1.0 Introduction and test results summary

The National Acoustic Laboratories were commissioned by REHAU to measure the acoustical transmission loss of a Tilt and Turn Window with 60mm PVC frame with steel reinforcing and 10.38mm glazing as described in item 2.0 'Test sample' details

The test sample achieved the following results :

Sound Transmission Class	STC 36
ISO-717 Sound Insulation Rating Rw (C; Ctr)	36 (-1 ; -2)
Outdoor Indoor Transmission Class	OITC 33
Unweighted average transmission loss value (100Hz - 5kHz)	35dB
A-Weighted average transmission loss value (100Hz - 5kHz)	30dB

2.0 Test sample details


Frame Type	Tilt and Turn window with fixed lite
Frame Material	PVC Frame with Steel reinforcing
Frame Dimensions	1150mm high x 1575mm wide
Glazing	10.38mm
Glazing Channels	EPDM Glazing seal
Lock/Latch Assembly	Tilt-turn gear set (ROTO)
Reveal Lining	20mm maple timber reveal
Installation	Sample screw fixed into a 1810mm wide x 1220mm high aperture with a 20mm thick maple timber reveal and sealed with silicone sealant. The PVC Secondary frame screw fixed and glued to the timber reveal with polyurethane sealant.
Drawing Number	LTB61 CM03
Test Date	10-Aug-2004
Notes	An extra wide timber reveal was fitted to the test window. This was because materials were not available at the time to manufacture a window of the correct size. Unfortunately this will have adversely affected the window's performance.

3.0 Testing rationale

The procedure for testing a small test sample building element such as a door or window requires the construction of a specially designed 'filler wall'. This filler wall is constructed in an aperture between two reverberation rooms and tested for acoustic transmission loss. After testing, an opening which is sufficiently large to accommodate the window or door is made in the filler wall (the size of the opening can be varied to suit a particular sample but normally it is 1850 x 1250mm (W x H) for windows and 1850 x 2150mm (W x H) for doors). The perimeter of this opening is lined with a layer of 16mm thick fire rated gypsum plasterboard, a layer of 12mm thick medium density fibreboard (m.d.f.) and a layer of Barium sulphate impregnated vinyl sheet. The small sample is then fitted into the opening and the acoustical integrity of the installation checked before testing.

The filler wall attenuation characteristics are designed to provide a minimum of 10dB greater attenuation than the test sample at all one-third octave frequencies between 80Hz and 5000Hz. This is to ensure an accurate measurement of the test sample according to standard acoustical practice, and to conform with the measurement requirements of AS1191-1985 *Acoustics - Method for laboratory measurement of airborne sound transmission loss of building partitions*. The transmission loss characteristics of this wall are presented in item 4.1 Sound Transmission Class of this report.

The second measurement taken is of the test sample fitted within the filler wall as presented in item 4.1 Sound Transmission Class of this report. The difference between the filler wall and filler wall and test sample measurements provide a means of calculating the Sound Transmission Class (STC) rating of the test sample as presented in item 4.1 Sound Transmission Class of this report. Other criteria presented in the report are derived from the two sets of measurements.

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4.0 Results

4.1 Sound Transmission Class

A complete set of measurements and calculations for determination of the test sample acoustical transmission loss was calculated and is presented numerically and graphically on the appended spreadsheets. A summation of one-third octave transmission loss results, rounded to the nearest deciBel (as required by AS1191-1985), follows.


Transmission Loss Measurement					
1/3 Octave Band Centre Frequency (Hz)	Filler Wall STC 80	Filler Wall and Test Sample STC 44	Test Sample STC 36	STC Criterion Value STC 36	Difference (dB)
80	41	35	29	-	-
100	50	32	25	-	-
125	59	35	27	20	-
160	60	33	26	23	-
200	65	36	29	26	-
250	71	40	33	29	-
315	73	40	32	32	-
400	76	42	34	35	-1
500	78	42	35	36	-1
630	80	43	36	37	-1
800	83	44	36	38	-2
1000	86	43	36	39	-3
1250	89	41	34	40	-6
1600	90	41	34	40	-6
2000	90	44	36	40	-4
2500	86	46	39	40	-1
3150	86	47	40	40	-
4000	92	51	43	40	-
5000	95	55	48	-	-
				SUM	-25

Note 1. The two channel pulse analyser averaging time conforms with the AS1191-1985 requirement of (1/20 the reverberation time of each one-third octave band in the measurement frequency range).

Note 2. Determination of Sound Transmission Class for a test sample requires comparison of the measured sound transmission loss with the value for each transmission class rating listed in the STC tables for each one-third octave band centre frequency, 125Hz to 4000Hz. The STC value, which is expressed as a class rating only (not as deciBels) as determined by these tables, is reached when either or both of the following requirements are met:

- (a) The test sample transmission loss at any frequency in the range 125Hz to 4000Hz must not lie more than 8dB below that of the STC reference graph value at the same frequency and
- (b) The total sum obtained from the addition of unfavourable deficiencies (as defined in the "Rw determination" description), must not add to more than 32dB. They are listed in the STC table above.

Note 3. Refer to the spreadsheet summaries (attached) for deciBel precision at the 95% confidence level for each attenuation value. The uncertainties have been calculated on the basis of there being not more than five chances in one hundred that any value differs from the true value by more than the stated uncertainty.

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4.2 Outdoor-Indoor Transmission Class

The first column of the Summarised OITC Rating Table lists centre frequencies of the one-third octave bands measured.

The second column specifies levels of the A-weighted reference spectrum defined by ASTM E1332 which are required to determine OITC. This spectrum has been A-Weighted and then normalised so that its energy summation is 0dB as required by that Standard.

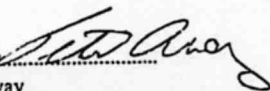
The third column contains transmission loss coefficients for each one-third octave band in the frequency range 80Hz to 4000Hz used to determine test sample OITC rating.

The fourth column represents the difference between column two and three converted to sound energy. The summation of this energy, converted back to deciBels is taken as the OITC value of the test sample.

OITC Rating			
1/3 Octave Band Centre Frequency (Hz)	Normalised A-Weighted Spectrum (dB)	Test Sample Transmission Loss (dB)	Transmitted Sound Energy (Watts)
80	-19.6	29	1.380E-05
100	-17.2	25	6.026E-05
125	-15.2	27	6.026E-05
160	-15.5	26	7.079E-05
200	-14	29	5.012E-05
250	-13.7	33	2.138E-05
315	-12.7	32	3.388E-05
400	-11.9	34	2.570E-05
500	-10.3	35	2.951E-05
630	-11	36	1.995E-05
800	-10.9	36	2.042E-05
1000	-11.1	36	1.950E-05
1250	-10.5	34	3.548E-05
1600	-11.1	34	3.090E-05
2000	-10.9	36	2.042E-05
2500	-11.8	39	8.318E-06
3150	-13.9	40	4.074E-06
4000	-15.1	43	1.549E-06
Sum of total energy =			5.263E-04
OITC = -10 * log (Sum of total energy) =			32.79
OITC			33

4.3 ISO-717 Sound Insulation Rating

Rw Rating	
Rw	36
C _T	-1
C _{TR}	-2

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5.0 Procedure for measuring test samples

The procedural detail requires reverberation room measurements of the following parameters for the filler wall and then for the filler wall with test sample fitted:

- Reverberation time measured in the receive room
- Sound pressure level in the send room and
- Sound pressure level in the receive room

The receive room reverberation time is measured according to the requirements of AS 1045 - 1985 "Acoustics - Measurement of Sound Absorption in a Reverberation Room". The procedures require twelve measurements of sound pressure levels in the send room and twelve in the receive room for each one-third octave band at different locations in the rooms.

Measurement of twenty four sets of sound decay data in the receive room requires the use of two sound sources, each positioned at a different location in the room and by moving the microphone through three positions, one for each measurement. A measurement is repeated four times for each combination of microphone and sound source location.

The total number of measurements required to evaluate sound pressure performance of the small test sample therefore comprises forty eight one-third octave sets of recordings in the send and receive rooms for the filler wall and forty eight sets for the filler wall with test sample installed. A set of recordings contains a measurement of the sound pressure level in each one-third octave frequency band between 100Hz and 5000Hz (eighteen in total), 80Hz is added to this for the calculation of OITC. These multiple measurements provide a means of calculating the sound field space-time variation within each room and establishes a basis for determining an estimation of the measurement precision to a confidence level of 95%.

Before testing commences, the measurement microphone in each reverberation room is acoustically calibrated and the acoustical noise floor measured. Acoustical calibration of each microphone is repeated at completion of the testing programme to ensure accuracy of results.


AS1191-1985 and the equivalent standards ISO140-1 and ISO140-3 describe procedures which allow measurement of transmission loss of 10 square metre samples or of smaller size samples such as windows, doors, partitions etc. The procedure for 10 square metre test samples is straightforward and requires only the aforementioned three sets of measurements. The procedure for measurement of smaller test samples, which is discussed in appendix A of AS1191-1985, requires construction and transmission loss measurement of a 10 square metre test wall which has at least 5dB and preferably 10dB more attenuation at each one-third octave band centre frequency in the frequency range to be measured than that of the smaller test sample to be evaluated and a calculation based on relative sizes of the 10 square metre test wall and the small test sample.

OITC is then calculated as required by ASTM E1332-90 by assuming the previously specified spectra and using the transmission loss coefficients obtained in the calculation procedure (refer spreadsheets) and R_w (C ; C_{tr}) calculated according to requirements of ISO 717-1:1996 "Acoustics - Rating of sound insulation in buildings and of building elements - Part 1: Airborne Sound Insulation".

6.0 Test sample performance assessment

Several criteria are presented in this report to evaluate the acoustical transmission loss of the test sample to satisfy building industry requirements in Australia. Each evaluation is made on an analysis of the calculated difference between the filler wall and the filler wall with test sample fitted.

- a. The Internationally used rating of Sound Transmission Class as required by Australian Standard AS1191-1985.
- b. The Weighted Sound Reduction Index, R_w rating with spectral corrections C and C_{tr} as discussed in International Standards Organisation document ISO717-1:1996 "Acoustics - Rating of sound insulation in buildings and of building elements - Part 1: Airborne Sound Insulation". The ISO R_w rating is relevant where the spectra has low frequency energy content and is similar in application to the American OITC criteria. They differ however in the frequency range of application. Each compares a standardised reference curve with the measured data over one-third octave bands. The R_w evaluation is carried out using the one-third octave band with centre frequencies ranging from 100Hz to 3150Hz, and the OITC evaluation is carried out using the one-third octave bands in the frequency range 80Hz to 4000Hz. The R_w criteria is now largely favoured as a replacement for STC. The OITC evaluation is included in our reports for clients who wish to market their products overseas.
- c. Other ratings presented are an evaluation of linear and A-weighted sound transmission loss averaged over the frequency range 100Hz to 5kHz. These are often required for marketing in New Zealand.

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7.0 Sound Transmission Class (STC) rating

The first criterion presented, Sound Transmission Class (STC), has been an internationally standardised criterion for many years for evaluating noise reducing characteristics of building elements. The test procedure provides a single number which has been considered sufficient to determine transmission loss of building elements such as walls, windows, doors and other small test samples fitted into the walls of buildings.

This STC rating criterion was originally developed for acoustical performance evaluation of internal walls and doors in buildings and is based on noise spectra with an energy distribution typical of music and speech. It is now considered to be unsuitable for use where the building element under evaluation is likely to be exposed to low frequency components of noise generated by transportation movement.

Determination of Sound Transmission Class for a test sample requires comparison of the measured sound transmission loss with the value for each transmission class rating listed in the STC tables for each one-third octave band centre frequency, 125Hz to 4000Hz. The STC value, which is expressed as a class rating only (not as deciBels) as determined by these tables, is reached when either or both of the following requirements are met:

- (a) The test sample transmission loss at any frequency in the range 125Hz to 4000Hz must not lie more than 8dB below that of the STC reference graph value at the same frequency and
- (b) The total sum obtained from the addition of unfavourable deficiencies (as defined in the "Rw determination" description), must not add to more than 32dB.

8.0 Outdoor - Indoor Transmission Class (OITC), and Rw (C; Ctr) Weighted Sound Reduction Ratings

Alternative single number criterion, the American Outdoor - Indoor Transmission Class (OITC) rating and the European International Organisation for Standardisation Document ISO 717-1:1996, specification for the Weighted Sound Reduction Index (Rw) associated with relevant spectrum corrections C and Ctr, have been developed in order to more closely rank transmission loss performance of building elements with a listener's subjective reaction to transportation and living activity type noise spectra. Each criterion is intended for use in situations where the relevant spectra can be transmitted through the element.


The OITC and Rw (C; Ctr) criterion are not considered to be suitable for use where the noise has a predominantly low frequency component such as produced by some industrial activities. More information on the OITC test procedure can be obtained in ASTM Standard Test Procedure E1332, "Standard Classification for Determination of Outdoor-Indoor Transmission Class" and the Weighted Sound Reduction Index, C and Ctr criteria are fully explained in ISO 717-1:1996, "Acoustics - Rating of sound insulation in buildings and of building elements - Part 1: Airborne Sound Insulation".

8.1 OITC determination

The OITC value for a test sample, as detailed in ASTM E 1332, is obtained by A-Weighting a noise spectrum which was obtained as an average of multiple measurements of aircraft take-off, freeway and railroad passby activities. This standardised noise spectrum is assumed to be in the send room during measurement of transmission loss.

The noise energy from this assumed noise spectra is (theoretically) transmitted through the small test sample, reduced by the transmission loss of the test sample at each one-third octave centre frequency (each transmission loss obtained from the STC measurement) and then summed as the total energy in the receive room.

The total energy is then determined as sound power (deciBels re 1 pW) and the resulting numerical value expressed as the OITC value of the sample under test. It should be noted that the OITC rating is considered as a class evaluation and stated numerically in a similar way to the STC value which is also a class evaluation (that is, stated numerically and not as deciBels as is sometimes found in literature).

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8.2 Rw determination

The Rw criterion is obtained by comparing the set of test sample transmission loss against a set of reference data specified on table 3 on page 4 of ISO 717-1: 1996 (the comparison is made between values specified for each set at each one-third octave band centre frequency over the frequency range 100Hz to 3150Hz).

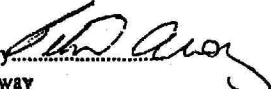
The reference data must then be amplitude shifted by the same amount (in single deciBel steps) until the sum of unfavourable readings, determined from the data difference at each frequency, is as large as possible but not more than 32dB. The 500Hz value of the reference data minus the number of decibels the reference data set has been shifted is then referred to as the Rw value for the test sample.

- Note 1. An unfavourable difference (deficiency) at any frequency occurs when the test sample transmission loss is less than the value specified for the shifted reference data at the same frequency.
- Note 2. The STC rating determination criterion has failure modes of -8dB at any one frequency and/or a deficiency sum of -32dB, whereas Rw has only a single failure mode, this being a -32dB deficiency summation over the pass band consisting of 100Hz to 3150Hz one-third octave bands. As a result of this, the Rw rating usually has the same numerical value as the STC rating unless the STC evaluation is a consequence of one or more -8dB deficiencies and any deficiency at 100Hz does not contribute to the Rw failure or at 4kHz to the STC failure.

8.3 C and Ctr determination

Rw corrections are accommodated in ISO 717-1:1996 to account for the type of spectra incident on the high noise side of a test sample. The correction C is applied to Rw spectra which is generated by sources such as transportation which are located close to the building element under test. Such noise sources have a wide energy distribution in their noise spectra. The correction Ctr is applied to pink noise or to spectra which is generated by sources such as transportation, located at a distance. This correction is applied to Rw where spectral energy is mostly concentrated in the low frequency end of the measurement frequency range.

Relevant Spectrum "correction" for different types of noise source (table A.1 of ISO717-1:1996)	
Type of Noise Source	Relevant Spectrum "Correction" Term
Living activities (talking, music, radio, TV) Children playing Railway traffic at medium and high speed Highway road traffic > 80km/hour Jet aircraft, short distance Factories emitting mainly medium and high frequency noise	C
Urban road traffic Railway traffic at low speeds Aircraft, propeller driven Jet aircraft, large distance Disco music Factories emitting mainly low and medium frequency noise	Ctr

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9.0 Test environment

Transmission loss measurement according to the requirements of AS1191 requires the use of two reverberation rooms which conform to the acoustical performance requirements of Annex D, guidelines for the design of reverberation rooms, ISO 3741-1975 "Acoustics - Determination of sound power levels of noise sources - Precision methods for broad-band sources in reverberation rooms".

Each test room, designated Reverberation (send) Room and Diffuse Field (receive) Room has a volume of approximately 200 cubic metres and is individually air conditioned by a special purpose acoustically attenuated air conditioning system. During testing, the supply and return air ducts are closed off via both pneumatically and manually operated dampers. The floors have different dimensions and are pentagonally shaped. The ceilings are inclined to the plane of the floor, opposite wall surfaces are different dimensions and inclined at an angle to each other to avoid acoustical coupling between rooms and to minimise the possibility of resonance in each room.

Additional sound diffusion within each of the rooms, to meet diffusivity requirements of ISO 354 - 1985 "Acoustics - Measurement of sound absorption in a reverberation room" is achieved by non-parallel room surfaces together with careful placing of eight 2400mm x 1200mm randomly oriented, freely suspended panels (19mm thick plywood sheets) with a total surface area of 40 square metres. These surfaces are heavily coated with epoxy resin to minimise acoustical absorption. The panels in each room are suspended in accordance with the tuning detail of ISO 354-1985 and therefore fully comply with the requirements of Australian Standard AS1045-1988.

Acoustical absorption coefficients in each octave band for each room and its diffusers do not exceed the maximum AS1191 requirement of 0.06 and are as follows:

Acoustical Absorption Coefficients						
Frequency	125Hz	250Hz	500Hz	1000Hz	2000Hz	4000Hz
Reverberation Room	0.02	0.01	0.02	0.03	0.04	0.06
Diffuse Field Room	0.02	0.02	0.02	0.03	0.04	0.06

Both reverberation rooms are inside separate isolating rooms, which serve as plenum chambers. This construction ensures freedom from flanking noise transmission problems even when very high acoustical sound pressure levels are generated inside either reverberation room.

The 300mm thick walls, floor and ceiling of all three rooms and plenum chambers are made from a heavily reinforced, high density concrete. The reverberation rooms are vibrationally suspended on damped, high tensile springs resting on neoprene rubber. The entire suspension assembly forms a two pole resonant suspension system, which is tuned below 5Hz.

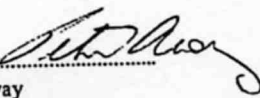
The complete mounting system of springs, dampers and high compliance acoustical seals around the test aperture ensures negligible vibrational coupling between the reverberation rooms or interference from outside vibrational sources for all frequencies within the operating range of the two reverberation rooms. Entry to both reverberation rooms and plenum chambers is by means of double doors.

Each room size, geometry and suspended diffusers ensures that the acoustical performance characteristics fully meet requirements of Australian Standard AS1191-1985.

A sample testing space of approximately 10 square metres is located within an opening in the common wall between the plenum chambers. This wall is part of the external sound shell construction, it is not a component of either test room and effectively isolates the sample from any vibrational energy, which may be generated inside either reverberation test room.

Exposure of either side of any test sample in this test space to a sound field is achieved via apertures in each reverberation room wall which align with the opening in the common wall of the plenum chambers. Acoustical sealing at the location of the openings between the reverberation rooms and the wall holding the test sample is achieved by means of compliant, high transmission loss and vibration isolation gaskets installed between the reverberation rooms and the common wall between the plenum chambers.

When testing small samples a filler wall is constructed in the 10 square metre opening in the testing space. An aperture is made in the filler wall, the test sample is then fitted and sealed in the opening. The acoustical integrity of the fitting is then tested.

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10.0 Formulae

(A) Receive room acoustical absorption

Sound absorption coefficients at each frequency band for the test specimen alpha (A) is determined from the reverberation time measurements according to the following equation:

$$A = \frac{0.16V}{T_{60}} \dots\dots(1)$$

Where

- A = the equivalent absorption area in the receiving room
- V = the receive room volume (in m³)
- T₆₀ = the receive room reverberation time (RT60)

(B) Average sound pressure level

Average sound pressure level (L_p) is determined for each frequency band as follows:

$$L_p = 10 \text{Log} \left[\frac{p_1^2 + p_2^2 + p_3^2 \dots\dots + p_n^2}{np_0^2} \right] \dots\dots(2)$$

Where

- L_p = Average sound pressure level (dB)
- p_n = sound pressure of the nth measurement (Pascals)
- p₀ = reference sound pressure (Pascals)
- n = number of measurements

(C) Transmission Loss

Since the sound fields in both rooms are diffuse and the environment is free of flanking transmission, sound transmission loss (R) of a test sample for each frequency band is calculated according to the following equation:

$$R = L_{pr} - L_{pr} + 10 \text{Log} \left[\frac{S}{A} \right] \dots\dots(3)$$

Where

- R = the sound transmission loss of the test sample
- L_{ps} = the average SPL in the source room
- L_{pr} = the average SPL in the receiving room
- S = the area of the specimen under test
- A = the equivalent absorption area in the receiving room

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(D) Small Test Samples

Test objects comprising a small size test sample mounted in a filler wall are measured according to the small sample method discussed in standard AS1191-1985. The equations used to calculate results are as follows:

Transmission loss coefficients for the small test sample (τ) are determined from the difference between the filler wall transmission loss (τ_c) and the composite wall transmission loss (τ_s) according to the following equations:

$$\tau_f = 10^{\frac{R_f}{10}} \dots\dots\dots(4)$$

$$\tau_c = 10^{\frac{R_c}{10}} \dots\dots\dots(5)$$

Rearranging the equations produces the transmission loss coefficient for each frequency band as follows:

$$\tau_s = \frac{\tau_c S_c - \tau_f S_f}{S_s} \dots\dots\dots(6)$$

Transmission loss for each frequency band (R_s) is determined from this result according to the following equation:

$$R_s = 10 \text{Log} \left[\frac{1}{\tau_s} \right] \dots\dots\dots(7)$$

Where

- τ_c = the transmission loss coefficient of the filler wall and the small test sample
- τ_f = the transmission loss coefficient of the filler wall
- τ_s = the transmission loss coefficient of the small test sample for each frequency band
- R_c = the transmission loss of the filler wall and the small test sample
- R_f = the transmission loss of the filler wall
- R_s = the transmission loss of the small test sample for each frequency band
- S_c = the surface area of the composite wall
- S_f = the surface area of the filler wall
- S_s = the surface area of the wall mounted small test sample

(E) Errors

Errors (95% confidence level) are determined for each frequency band by means of the following equation:

$$\text{Error}(95\% \text{confidence}) = \frac{t \cdot sd}{\sqrt{n}} \dots\dots\dots(8)$$

Where

- n = the number of microphone positions sampled
- t = the students t factor
- sd = the standard deviation obtained from the measurement spreadsheet

11.0 Instrumentation

The following instrumentation is used for acoustical transmission loss measurements. Instrumentation calibration where appropriate has been calibrated according to NATA requirements.

- Brüel and Kjaer two channel pulse analyser (assembly 2825, 7521, 2 x 3015), S/N 2005502
- Brüel and Kjaer Cathode Follower type 2639, S/N 1448239 & S/N 1391974
- Brüel and Kjaer Cathode Follower type 2660, S/N 1337994 & S/N 1338051
- Brüel and Kjaer Cathode Follower type 2669, S/N 1888716 & S/N 1834203
- Brüel and Kjaer Microphone type 4144, S/N 563123, S/N 1138528, S/N 439142 & S/N 2118354
- Brüel and Kjaer Microphone type 4179, S/N 2245299, S/N 2245300 & S/N 2245154
- Brüel and Kjaer Sound Level Calibrator type 4231, S/N 2095393
- Yamaha Professional Sound Sources type S500, S/N 1068 and S/N 1069
- Murray 100 Watt Amplifier type MA534, S/N 15
- Vaisala Digital Barometer type PTB201AD, S/N R3330001
- Testo Temperature/Humidity Logger, type 177-H1, S/N 00886924

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ATF Report 1547

Client Name: REHAU

Testing Officer: Peter Alway

FILLER WALL ONLY

Test Conditions:
 Total Area Under Test (Sq m): 9.37
 Biometric Air Pressure (hPa): 1016
 Temperature (C): 16.8
 Relative Humidity SR (%): 65.4
 Receive Room Volume (Cu m): 200
 Relative Humidity RR (%): 65.4
 Speed of Sound (m/s): 342.16

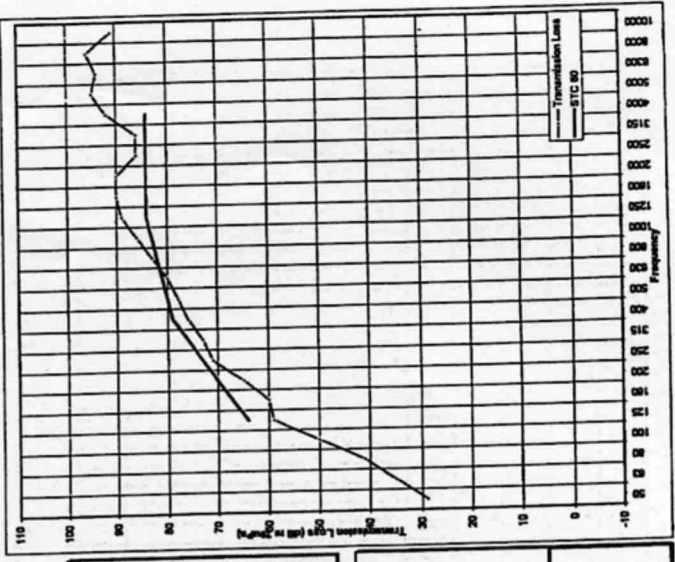
Date Of Test: 9-Aug-2004

Signature: *Peter Alway*
 Peter Alway.

Frequency	Mean SEND Room SPL (dB)	Mean RECEIVE Room SPL (dB)	Difference with Mic Responses	Mean Receive Room Reverb RT60 (seconds)	10*log (S/A)	10*log (S/R)	10*log (S/A) - 10*log (S/R)	Calculated 1/3 Octave Transmission Loss (dB)	Calculated 1/1 Octave Transmission Loss (dB)
80 Hz	80.50	1.30	51.45	1.87	29.08	3.42	0.28	29.338	33.048
100 Hz	80.47	2.04	44.60	3.22	35.80	2.64	-0.54	35.288	33.048
125 Hz	80.47	2.04	44.60	3.22	35.80	2.64	-0.03	40.747	33.048
160 Hz	87.15	1.81	39.69	2.10	40.78	3.19	1.49	50.390	55.416
200 Hz	86.00	1.84	38.25	2.38	43.90	4.32	2.03	58.888	55.416
250 Hz	87.17	1.28	31.36	1.16	38.53	6.09	5.28	59.715	55.416
315 Hz	87.05	0.87	30.24	0.91	38.94	8.09	4.65	66.982	55.416
400 Hz	87.85	0.87	26.17	1.30	37.78	8.86	3.31	71.058	55.416
500 Hz	88.54	0.88	21.09	0.88	37.45	7.30	4.08	72.503	55.416
630 Hz	88.83	0.88	19.99	0.82	36.84	7.30	4.08	75.572	55.416
800 Hz	91.65	0.43	19.86	0.62	36.84	7.11	3.80	77.989	55.416
1000 Hz	92.88	0.33	18.00	0.31	33.79	7.68	3.78	79.887	55.416
1250 Hz	91.54	0.32	15.05	0.31	31.77	7.08	3.44	83.444	55.416
1600 Hz	91.54	0.32	11.54	0.39	30.40	6.47	3.04	83.720	55.416
2000 Hz	95.27	0.34	12.45	0.41	30.80	6.30	2.93	88.758	55.416
2500 Hz	98.56	0.34	11.61	0.38	32.78	5.74	2.52	90.289	55.416
3150 Hz	100.83	0.35	11.61	0.38	32.78	4.80	1.75	90.029	55.416
4000 Hz	98.32	0.38	9.67	0.27	30.10	3.98	0.93	88.950	55.416
5000 Hz	97.55	0.41	8.58	0.20	28.13	2.55	-1.00	86.122	55.416
6300 Hz	98.03	0.46	2.03	0.31	33.24	2.18	-1.69	91.559	55.416
8000 Hz	97.69	0.47	-4.02	0.28	32.82	1.85	-2.40	95.410	55.416
10000 Hz	98.00	0.42	-5.22	0.22	30.82	1.77	-2.50	93.515	55.416
12500 Hz	98.00	0.36	-4.40	0.24	30.84	1.87	-2.34	96.378	55.416
16000 Hz	90.30	0.38	-7.30	0.18	33.52	1.88	-2.32	91.199	55.416

Material Under Test:
 Filler wall for window test program August 2004

Arithmetic Average of Transmission Loss From 100Hz to 5kHz
 Unweighted Average: 78
 A-Weighted Average: 74



1/1 Octave

Frequency	Rounded 1/1 Octave Transmission Loss Values (dB)
63 Hz	33
125 Hz	55
250 Hz	60
500 Hz	77
1000 Hz	87
2000 Hz	91
4000 Hz	92
8000 Hz	99

Rw Rating
 Rw = 79
 C₁ = -4
 C₂ = -10
 C₁ (50-5000) = -12
 C₂ (50-5000) = -27
 Ref (C₁, C₂) is 79 (-4; -10)
 Ref (C₁, C₂) (50-5000) is 79 (-4; -10; -12; -27)

OITC Rating

Frequency	Normalized A-Weighted Reference Spectrum (dB)	Sound Energy (Wind)
80 Hz	-19.8	6.710E-07
100 Hz	-17.2	1.905E-07
125 Hz	-15.2	3.802E-08
160 Hz	-15.5	2.818E-08
200 Hz	-14	1.259E-08
250 Hz	-13.7	3.398E-09
315 Hz	-12.7	2.692E-09
400 Hz	-11.9	1.822E-09
500 Hz	-10.3	1.478E-09
630 Hz	-11	7.943E-10
800 Hz	-10.9	4.074E-10
1000 Hz	-11.1	1.950E-10
1250 Hz	-10.5	1.122E-10
1600 Hz	-11.1	7.782E-11
2000 Hz	-10.9	6.128E-11
2500 Hz	-11.8	1.860E-10
3150 Hz	-13.9	1.023E-10
4000 Hz	-15.1	1.850E-11
Sum	-10*log(Sum)	59.39

The Outdoor Indoor Transmission Class is:
OITC 59

Results (incorporating AS1191-1985 Compliant Measurements)

Frequency	Rounded 1/3 Octave Transmission Loss Values (dB)	STC 80 Curve	Transmission Loss to STC Difference
50	29	64	-5
63	35	67	-7
80	41	70	-5
100	50	73	-2
125	59	76	-3
160	60	79	-3
200	65	80	-2
250	71	81	-1
315	73	82	-
400	76	83	-
500	78	84	-
630	83	84	-
800	86	84	-
1000	89	84	-
1250	90	84	-
1600	90	84	-
2000	90	84	-
2500	86	84	-
3150	86	84	-
4000	92	84	-
5000	95	84	-
6300	94	84	-
8000	96	84	-
10000	91	84	-
Sum	-28		

The Sound Transmission Class Of This Sample is:
STC 80

ATC 1616 Window Transmission Loss August 2004 via Filler Wall Results

ATF Report 1549

Client Name: REHAU

FILLER WALL + SAMPLE

Testing Office: Peter Alway

Total Area Under Test (Sq m): 8.87
 Temperature (C): 18.6
 Relative Humidity SR (%): 48.3
 Relative Humidity RR (%): 48.3
 Receiver Room Volume (Cu m): 200
 Speed of Sound (m/s): 342.18

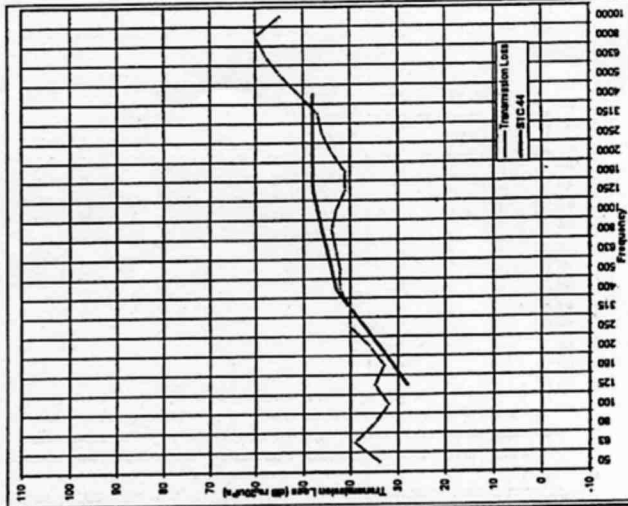
Date of Test: 10-Aug-2004

Signatory: Peter Alway

Frequency	Mean SEND Room SPL (dB)	Mean RECEIVE Room SPL (dB)	Differences with Mic Responses Corrections	Mean Receive Room Reverb RT60 (seconds)	10*log (SIA) dB	Frequency	Precision 1/1 Octave Transmission Loss (dB)	Calculated 1/1 Octave Transmission Loss (dB)
63 Hz	83.72	48.11	35.61	2.75	-0.67	63 Hz	2.84	33.038
125 Hz	82.78	43.02	39.76	2.58	-0.94	125 Hz	3.20	31.229
250 Hz	81.26	31.6	49.66	2.91	-0.43	250 Hz	2.35	35.048
500 Hz	86.81	35.38	51.43	3.49	0.38	500 Hz	1.79	31.885
1000 Hz	86.05	33.59	52.46	3.26	1.10	1000 Hz	1.58	34.079
2000 Hz	85.73	31.35	54.38	3.00	1.82	2000 Hz	1.58	33.271
4000 Hz	85.35	28.81	56.54	2.88	2.48	4000 Hz	0.75	40.488
8000 Hz	84.20	26.34	57.86	2.71	3.48	8000 Hz	0.41	41.857
10000 Hz	83.45	24.81	58.64	2.65	3.74	10000 Hz	0.38	42.288
125 Hz	84.25	44.87	39.38	7.60	3.38	125 Hz	0.38	43.538
250 Hz	83.48	42.72	40.76	6.30	2.83	250 Hz	0.35	43.888
500 Hz	85.35	45.09	40.26	5.97	2.69	500 Hz	0.35	42.853
1000 Hz	87.67	48.32	39.35	5.52	2.35	1000 Hz	0.35	41.482
2000 Hz	88.60	46.36	42.24	4.56	1.83	2000 Hz	0.36	43.888
4000 Hz	85.27	37.66	47.61	3.85	0.79	4000 Hz	0.36	48.253
8000 Hz	84.03	34.26	49.77	3.24	0.04	8000 Hz	0.43	47.353
10000 Hz	81.91	20.56	61.35	2.78	-0.83	10000 Hz	0.64	50.788
125 Hz	79.25	12.54	66.71	2.30	-1.45	125 Hz	0.90	55.114
250 Hz	78.05	9.05	68.99	1.89	-2.34	250 Hz	0.90	58.139
500 Hz	71.71	0.47	71.24	0.87	-4.88	500 Hz	0.92	58.837
10000 Hz			81.10	0.87	-5.88	10000 Hz	0.94	55.438

Radical Under Test:
 80mm IR and turn window with steel reinforcing
 10.30mm glass

Arithmetic Average of Transmission Loss From 100hz to 5kHz
 Unweighted Average: 42
 A-Weighted Average: 38



1/1 Octaves

Frequency	Rounded 1/1 Octave Transmission Loss Value (dB)
63 Hz	38
125 Hz	34
250 Hz	38
500 Hz	42
1000 Hz	43
2000 Hz	44
4000 Hz	52
8000 Hz	64

Rw Rating
 Rw = 44
 C1 = -1
 C2 = -3
 C3 (50-500) = 0
 C4 (50-1000) = -3
 Ref C1; C2; C3; C4 is 44 (-1; -3)
 Ref C1; C2; C3; C4; C5; C6; C7; C8; C9; C10 is 44 (-1; -3; 0; -3)

OITC Rating

Frequency	Normalized A-Weighted Reference Noise Spectrum (dB)	Sound Energy (mJ/m²)
63 Hz	-19.6	3.467E-06
125 Hz	-17.2	1.202E-05
250 Hz	-15.5	8.550E-05
500 Hz	-14	1.413E-04
1000 Hz	-13.7	1.000E-04
2000 Hz	-12.7	4.268E-05
4000 Hz	-11.9	4.074E-05
8000 Hz	-10.3	5.888E-05
10000 Hz	-11	3.981E-05
125 Hz	-10.9	3.890E-05
250 Hz	-11.1	7.078E-05
500 Hz	-10.5	1.188E-04
1000 Hz	-11.1	5.188E-05
2000 Hz	-10.9	3.288E-05
4000 Hz	-11.8	1.800E-05
8000 Hz	-13.9	5.188E-07
10000 Hz	-15.1	2.485E-07
Sum		9.907E-06
-1*Log10(sum)		40.04

The Outdoor Indoor Transmission Class is:
OITC 40

Results In accordance with AS1181-1995 Compliant Measurements

Frequency	Rounded 1/2 octave Transmission Loss Value (dB)	STC 44 Curve	Transmission Loss to STC Difference
50	34		
63	34		
80	35		
100	32	28	
125	35	31	
160	33	34	
200	38	37	
250	40	40	
315	40	43	
400	42	44	-1
500	42	45	-2
630	44	46	-2
800	44	47	-3
1000	43	48	-4
1250	41	48	-7
1600	41	48	-4
2000	44	48	-4
2500	48	48	-2
3150	47	48	-1
4000	51	45	
5000	55		
6300	58		
8000	60		
10000	55		
Sum			-32

The Sound Transmission Class of This Sample is:
STC 44

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ATF Report 1549

Client Name: **REHAU**

SAMPLE ONLY

Surface Area Of Test Sample (Sq. m): **1.811**
 Surface Area Of Remaining Filler Wall: **8.159**
 Total Surface Area Of Test Aperture: **9.97**

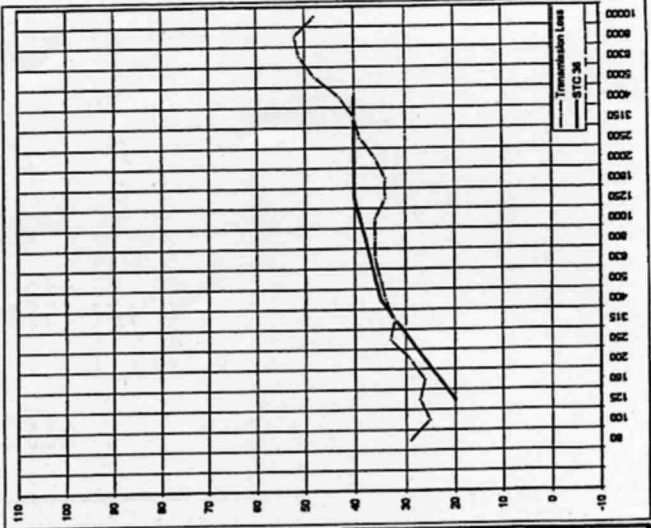
Test Conditions:
 Date Of Test: **10-Aug-2004**

Signature: *[Signature]*
 Peter Alway.

Frequency	Filler Wall Transmission Loss (dB)	Filler Wall Sample Transmission Loss	Transmission Coefficient of Filler Wall (%)	Transmission Coefficient of Sample (%)	1/T _s	Calculated 1/3 Octave Transmission Loss (dB)	Prediction 95% Confidence Interval (dB)	Calculated 1/1 Octave Transmission Loss (dB)
80 Hz	40.75	35.05	2.28	8.41893E-05	744.42	28.718	3.04	28.718
100 Hz	50.39	31.89	1.76	9.14024E-06	283.66	24.928	2.48	24.928
125 Hz	58.86	34.68	1.36	1.38258E-06	535.30	27.288	2.03	27.288
160 Hz	59.71	33.27	1.55	1.000470864	368.49	25.971	1.85	25.971
200 Hz	65.09	38.48	1.08	3.09635E-07	809.15	28.080	1.48	28.080
250 Hz	71.06	40.41	0.78	7.84211E-08	1998.95	33.004	0.81	33.004
315 Hz	72.90	39.85	0.78	5.12551E-08	1756.35	32.448	0.86	32.448
400 Hz	75.57	41.66	0.61	1.000103484	2680.08	34.250	0.84	34.250
500 Hz	78.89	42.22	0.58	1.77038E-08	3028.18	34.209	0.77	34.209
630 Hz	83.44	43.69	0.58	1.02846E-08	3857.77	35.532	0.69	35.532
800 Hz	85.72	42.85	0.42	4.92514E-09	4248.77	38.281	0.45	38.281
1000 Hz	88.76	41.49	0.31	2.87938E-09	3585.19	35.545	0.58	35.545
1250 Hz	90.29	41.40	0.38	1.33081E-09	2581.00	34.084	0.48	34.084
1600 Hz	90.03	43.81	0.38	9.35543E-10	2508.38	33.984	0.51	33.984
2000 Hz	85.85	46.29	0.33	8.83281E-10	4388.07	38.461	0.52	38.461
2500 Hz	86.12	47.30	0.43	2.60011E-09	7737.54	38.886	0.52	38.886
3150 Hz	91.58	50.80	0.38	2.44234E-09	8763.54	39.836	0.57	39.836
4000 Hz	95.41	55.11	0.38	8.99591E-10	21620.10	43.389	0.48	43.389
5000 Hz	93.52	55.11	0.48	2.87732E-10	69978.75	47.707	0.78	47.707
6300 Hz	96.38	58.64	0.48	4.45099E-10	110364.81	50.732	0.84	50.732
8000 Hz	91.20	55.44	0.48	2.30338E-10	167119.29	52.230	0.88	52.230
10000 Hz			0.48	7.58718E-10	63952.70	48.031	1.32	48.031

Sample Under Test:
 60mm lift and turn window with steel reinforcing
 10.38mm glass

Arithmetic Average of Transmission Loss From 100hz to 5khz
 Unweighted Average: **35**
 A-Weighted Average: **30**



1/1 Octave Rounded 1/1 Octave Transmission Loss Values (dB)

Frequency	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz	8000 Hz
Loss Value (dB)	27	32	35	38	43	49	57

OITC Rating

Frequency	80 Hz	100 Hz	125 Hz	160 Hz	200 Hz	250 Hz	315 Hz	400 Hz	500 Hz	630 Hz	800 Hz	1000 Hz	1250 Hz	1600 Hz	2000 Hz	2500 Hz	3150 Hz	4000 Hz
Normalized A-Weighted Reference Noise Spectrum (dB)	-19.6	-17.2	-15.2	-15.5	-14	-13.7	-12.7	-11.9	-10.3	-11	-10.9	-11.1	-10.5	-11.1	-10.9	-11.8	-13.9	-15.1
Sound Energy (W/m2)	1.380E-05	6.028E-05	6.028E-05	7.079E-05	5.012E-05	2.138E-05	3.308E-05	2.570E-05	2.951E-05	1.995E-05	2.042E-05	1.950E-05	3.548E-05	3.090E-05	2.042E-05	8.318E-06	4.074E-06	1.548E-06
Sum	-19*LOG(Sum) 32.79																	

Results (Incorporating AS1191-1985 Compliant Measurements)

Frequency	Rounded 1/3 Octave Transmission Loss (dB)	STC 36 Curve	Transmission Difference
80	29		
100	25		
125	27	20	-7
160	26	23	-3
200	29	26	-3
250	33	29	-4
315	32	32	-4
400	34	35	-1
500	35	36	-1
630	36	37	-1
800	36	38	-2
1000	36	39	-3
1250	34	40	-6
1600	34	40	-6
2000	36	40	-4
2500	39	40	-1
3150	40	40	-
4000	43	40	-3
5000	48		
6300	51		
8000	52		
10000	48		
Sum			-25

R_w Rating
 R_w = **36**
 C₁ = **-1**
 C₂ = **-2**

The Outdoor Indoor Transmission Class is:
OITC 33

The Sound Transmission Class Of This Sample is:
STC 36

Date: **30/8/04**
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ATF Report 1549

Date Of Test 10-Aug-2004

Rw Calculation Spreadsheet

R_{eq} = 36

Frequency (Hz)	Transmission Loss R _i (Proprietary data in 1 significant figure)	Rw 36 Curve	Transmission Loss to Rw Difference
100	24.5	17	-
125	27.3	20	-
160	25.9	23	-
200	29.1	28	-
250	33	29	-
315	32.4	32	-
400	34.3	35	-0.7
500	34.8	36	-1.2
630	36.3	37	-1.4
800	36.3	38	-1.7
1000	35.5	39	-3.5
1250	34.1	40	-5.9
1600	34	40	-6
2000	36.4	40	-3.6
2500	38.9	40	-1.1
3150	39.9	40	-0.1
SUM			-25.2

Determination Of Correction C_i

C spectrum (ISO 717-2)	L _i	L _i -R _i	10 ^A ((L _i -R _i)/10)
-28	-28	-53.50	4.487E-06
-28	-28	-53.30	4.877E-06
-23	-23	-48.90	1.266E-05
-21	-21	-60.10	9.772E-06
-19	-19	-52.00	6.310E-06
-17	-17	-48.40	1.148E-05
-15	-15	-49.30	1.178E-05
-13	-13	-47.80	1.600E-05
-12	-12	-47.80	1.738E-05
-11	-11	-47.30	1.662E-05
-10	-10	-46.50	2.518E-05
-9	-9	-43.10	4.898E-05
-9	-9	-43.00	5.012E-05
-8	-8	-45.40	2.864E-05
-8	-8	-47.90	1.622E-05
-9	-9	-48.90	1.288E-05
SUM			2.992E-04
10 ¹⁰ Log (SUM)			35.24

C = -1

Determination Of Correction C_{TR}

C _{TR} spectrum (ISO 717-2)	L _g	L _g -R _i	10 ^A ((L _g -R _i)/10)
-20	-20	-44.80	3.548E-05
-20	-20	-47.30	1.862E-05
-18	-18	-43.90	4.074E-05
-16	-16	-48.10	3.090E-05
-16	-16	-48.00	1.595E-05
-14	-14	-48.40	2.291E-05
-13	-13	-47.30	1.862E-05
-12	-12	-48.80	2.089E-05
-11	-11	-48.80	2.198E-05
-9	-9	-45.30	2.951E-05
-9	-9	-43.10	4.487E-05
-8	-8	-43.00	4.898E-05
-8	-8	-44.00	3.981E-05
-11	-11	-47.40	1.820E-05
-13	-13	-51.90	8.457E-06
-16	-16	-64.90	3.236E-06
SUM			4.188E-04
10 ¹⁰ Log (SUM)			33.80

C_{TR} = -2

Determination Of Arithmetic Average Of Transmission Loss

Frequency (Hz)	Calculated Transmission Loss	A-Weighting Correction	A-weighted Transmission Loss
100	24.528	-19.1	5.428
125	27.266	-16.1	11.166
160	25.871	-13.4	12.471
200	29.080	-10.9	18.180
250	33.004	-8.6	24.404
315	32.446	-6.9	25.546
400	34.260	-4.8	29.460
500	34.909	-3.2	31.609
630	35.632	-1.9	33.732
800	36.281	-0.8	35.481
1000	35.545	0	35.545
1250	34.084	0.6	34.684
1600	33.994	1	34.994
2000	36.401	1.2	37.601
2500	38.896	1.3	40.188
3150	39.896	1.2	41.096
4000	43.369	1	44.369
5000	47.707	0.5	48.207

Average = 34.616

A-weighted Average = 30.249

Rounded = 35

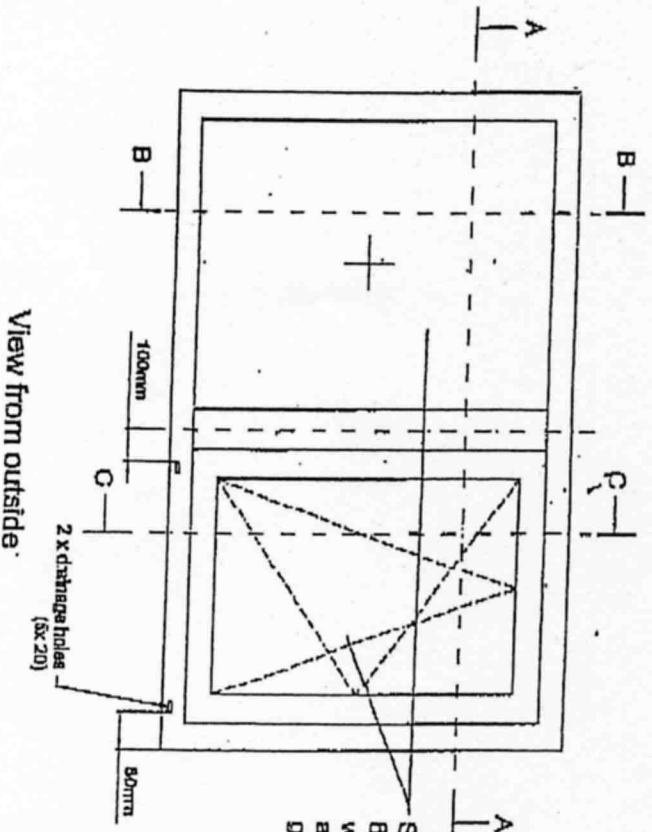
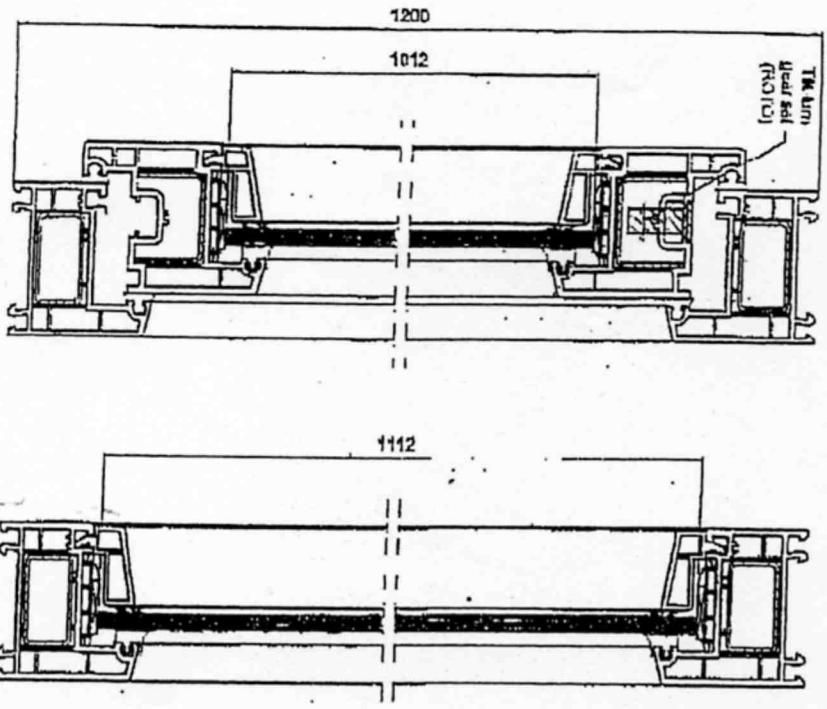
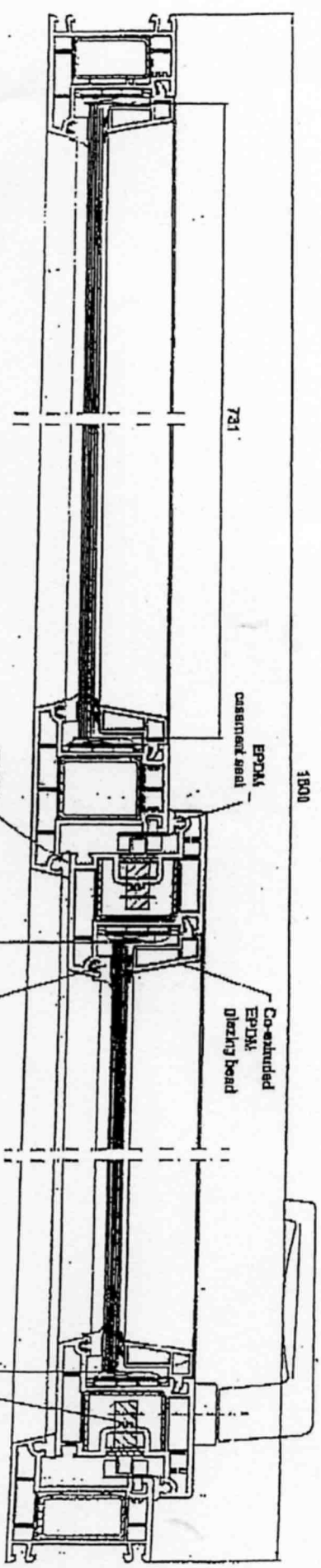
Rounded = 30

Signatory *Peter Alway*
Peter Alway.

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Date: 30/8/04

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Single glazed glass
6.38 laminated
with EPDM glazing seals
and co-extruded EPDM
glazing bead

REHAU		S921	
Scale: M 1 : 2		Prestige-Design	
Drawn by: Hochleitl	Tilt-turn gear on	Inward open window	
Dwg No.: LTB01 CM03	with fixed life with	Frame 60 & Sash 758	

Signatory: *[Signature]*
Peter Alway