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National Acoustic Laboratories

## ATF Report 1733

**Airborne Sound Transmission  
Test of a Casement Window  
with Fixed Light**

**Commissioned by  
Rehau**

**Test Date: 31st August 2005**



AS1191-2002, AS1045-1988  
Accredited Lab No: 5472

## Airborne Sound Transmission Test of a Casement Window with Fixed Light

### 1.0 Introduction and test results summary

The National Acoustic Laboratories were commissioned by Rehau to measure the acoustical transmission loss of a casement window with fixed light as described in item 2.0 'Test sample' details

The test sample achieved the following results :

Sound Transmission Class	STC 41
ISO-717 Sound Insulation Rating Rw (C; Ctr)	41 ( -2 ; -6 )
Outdoor Indoor Transmission Class	OITC 33
Unweighted average transmission loss value (100Hz - 5kHz)	38dB
A-Weighted average transmission loss value (100Hz - 5kHz)	34dB

### 2.0 Test sample details

<b>Frame Type</b>	Casement Window with fixed light
<b>Frame Material</b>	PVC
<b>Frame Dimensions</b>	1240mm x 1840mm
<b>Glazing</b>	IGU 10.38mm laminated glass on the send side, 16mm air gap then 6.76mm laminated glass on receive side
<b>Glazing Channels</b>	Art 500133
<b>Sash Seals</b>	Art 221866 Casement seal
<b>Lock/Latch Assembly</b>	Roto lock keeper & handle with Friction Stay 16" SS304
<b>Reveal Lining</b>	19mm timber reveal
<b>Installation</b>	Sample screw fixed into the test sample aperture with a 19mm thick timber reveal and all gaps packed and sealed with silicone sealant.

#### Test Date

31-Aug-2005

#### Notes

Due to the uncertainty at low frequencies the 63Hz figure was adjusted so that the measured figure didn't appear to have more loss than the original wall. Being as it is such a low frequency it does not affect the value of the Rw or CTR figure.

### 3.0 Testing rationale

The procedure for testing a small test sample building element such as a door or window requires the construction of a specially designed 'filler wall'. This filler wall is constructed in an aperture between two reverberation rooms and tested for acoustic transmission loss. After testing, an opening which is sufficiently large to accommodate the window or door is made in the filler wall (the size of the opening can be varied to suit a particular sample but normally it is 1850 x 1250mm (W x H) for windows and 1850 x 2150mm (W x H) for doors). The perimeter of this opening is lined with a layer of 16mm thick fire rated gypsum plasterboard, a layer of 12mm thick medium density fibreboard (m.d.f.) and a layer of Barium sulphate impregnated vinyl sheet. The small sample is then fitted into the opening and the acoustical integrity of the installation checked before testing.

The filler wall attenuation characteristics are designed to provide a minimum of 10dB greater attenuation than the test sample at all one-third octave frequencies between 80Hz and 5000Hz. This is to ensure an accurate measurement of the test sample according to standard acoustical practice, and to conform with the measurement requirements of AS1191-2002. *Acoustics - Method for laboratory measurement of airborne sound transmission loss of building partitions*. The transmission loss characteristics of this wall are presented in item 4.1 **Sound Transmission Class** of this report.

The second measurement taken is of the test sample fitted within the filler wall as presented in item 4.1 **Sound Transmission Class** of this report. The difference between the filler wall and filler wall and test sample measurements provide a means of calculating the Sound Transmission Class (STC) rating of the test sample as presented in item 4.1 **Sound Transmission Class** of this report. Other criteria presented in the report are derived from the two sets of measurements.

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#### 4.0 Results

##### 4.1 Sound Transmission Class

A complete set of measurements and calculations for determination of the test sample acoustical transmission loss was calculated and is presented numerically and graphically on the appended spreadsheets. A summation of one-third octave transmission loss results, rounded to the nearest deciBel (as required by AS1191-2002), follows.

Transmission Loss Measurement					
1/3 Octave Band Centre Frequency (Hz)	Filler Wall STC 82	Filler Wall and Test Sample STC 47	Test Sample STC 41	STC Criterion Value STC 41	Difference (dB)
80	48	33	27	-	-
100	55	27	21	-	-
125	63	28	22	25	-3
160	64	34	28	28	-
200	66	37	30	31	-1
250	73	38	32	34	-2
315	77	43	37	37	-
400	78	45	38	40	-2
500	82	46	39	41	-2
630	84	47	41	42	-1
800	85	47	41	43	-2
1000	87	48	42	44	-2
1250	90	47	41	45	-4
1600	89	46	40	45	-5
2000	81	46	40	45	-5
2500	81	49	43	45	-2
3150	87	53	46	45	-
4000	92	59	52	45	-
5000	91	64	58	-	-
SUM					-31

Note 1. The two channel pulse analyser averaging time conforms with the AS1191-2002 requirement of (1/20 the reverberation time of each one-third octave band in the measurement frequency range).

Note 2. Determination of Sound Transmission Class for a test sample requires comparison of the measured sound transmission loss with the value for each transmission class rating listed in the STC tables for each one-third octave band centre frequency, 125Hz to 4000Hz. The STC value, which is expressed as a class rating only (not as deciBels) as determined by these tables, is reached when either or both of the following requirements are met:

- (a) The test sample transmission loss at any frequency in the range 125Hz to 4000Hz must not lie more than 8dB below that of the STC reference graph value at the same frequency and
- (b) The total sum obtained from the addition of unfavourable deficiencies (as defined in the "Rw determination" description), must not add to more than 32dB. They are listed in the STC table above.

Note 3. Refer to the spreadsheet summaries (attached) for deciBel precision at the 95% confidence level for each attenuation value. The uncertainties have been calculated on the basis of there being not more than five chances in one hundred that any value differs from the true value by more than the stated uncertainty.

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**4.2 Outdoor-Indoor Transmission Class**

The first column of the Summarised OITC Rating Table lists centre frequencies of the one-third octave bands measured.

The second column specifies levels of the A-weighted reference spectrum defined by ASTM E1332 which are required to determine OITC. This spectrum has been A-Weighted and then normalised so that its energy summation is 0dB as required by that Standard.

The third column contains transmission loss coefficients for each one-third octave band in the frequency range 80Hz to 4000Hz used to determine test sample OITC rating.

The fourth column represents the difference between column two and three converted to sound energy. The summation of this energy, converted back to decibels is taken as the OITC value of the test sample.

OITC Rating			
1/3 Octave Band Centre Frequency (Hz)	Normalised A-Weighted Spectrum (dB)	Test Sample Transmission Loss (dB)	Transmitted Sound Energy (Watts)
80	-19.6	27	2.188E-05
100	-17.2	21	1.514E-04
125	-15.2	22	1.905E-04
160	-15.5	28	4.467E-05
200	-14	30	3.981E-05
250	-13.7	32	2.692E-05
315	-12.7	37	1.072E-05
400	-11.9	38	1.023E-05
500	-10.3	39	1.175E-05
630	-11	41	6.310E-06
800	-10.9	41	6.457E-06
1000	-11.1	42	4.898E-06
1250	-10.5	41	7.079E-06
1600	-11.1	40	7.762E-06
2000	-10.9	40	8.128E-06
2500	-11.8	43	3.311E-06
3150	-13.9	46	1.023E-06
4000	-15.1	52	1.950E-07
Sum of total energy =			5.530E-04
OITC = -10 * log (Sum of total energy ) =			32.57
			OITC 33

**4.3 ISO-717 Sound Insulation Rating**

Rw Rating	
Rw	41
C <sub>T</sub>	-2
C <sub>TR</sub>	-6
C <sub>T</sub> (50-5000)	-1
C <sub>TR</sub> (50-5000)	-6

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## 5.0 Procedure for measuring test samples

The procedural detail requires reverberation room measurements of the following parameters for the filler wall and then for the filler wall with test sample fitted:

- Reverberation time measured in the receive room
- Sound pressure level in the send room and
- Sound pressure level in the receive room

The receive room reverberation time is measured according to the requirements of AS 1045 - 1985 "*Acoustics - Measurement of Sound Absorption in a Reverberation Room*". The procedures require twelve measurements of sound pressure levels in the send room and twelve in the receive room for each one-third octave band at different locations in the rooms.

Measurement of twenty four sets of sound decay data in the receive room requires the use of two sound sources, each positioned at a different location in the room and by moving the microphone through three positions, one for each measurement. A measurement is repeated four times for each combination of microphone and sound source location.

The total number of measurements required to evaluate sound pressure performance of the small test sample therefore comprises forty eight one-third octave sets of recordings in the send and receive rooms for the filler wall and forty eight sets for the filler wall with test sample installed. A set of recordings contains a measurement of the sound pressure level in each one-third octave frequency band between 100Hz and 5000Hz (eighteen in total), 80Hz is added to this for the calculation of OITC. These multiple measurements provide a means of calculating the sound field space-time variation within each room and establishes a basis for determining an estimation of the measurement precision to a confidence level of 95%.

Before testing commences, the measurement microphone in each reverberation room is acoustically calibrated and the acoustical noise floor measured. Acoustical calibration of each microphone is repeated at completion of the testing programme to ensure accuracy of results.

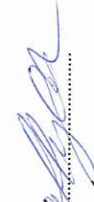
AS1191-2002 and the equivalent standards ISO140-1 and ISO140-3 describe procedures which allow measurement of transmission loss of 10 square metre samples or of smaller size samples such as windows, doors, partitions etc. The procedure for 10 square metre test samples is straightforward and requires only the aforementioned three sets of measurements. The procedure for measurement of smaller test samples, which is discussed in appendix A of AS1191-2002, requires construction and transmission loss measurement of a 10 square metre test wall which has at least 5dB and preferably 10dB more attenuation at each one-third octave band centre frequency in the frequency range to be measured than that of the smaller test sample to be evaluated and a calculation based on relative sizes of the 10 square metre test wall and the small test sample.

OITC is then calculated as required by ASTM E1332-90 by assuming the previously specified spectra and using the transmission loss coefficients obtained in the calculation procedure (refer spreadsheets) and Rw (C; Ctr) calculated according to requirements of ISO 717-1:1996 "*Acoustics - Rating of sound insulation in buildings and of building elements - Part 1: Airborne Sound Insulation*".

## 6.0 Test sample performance assessment

Several criteria are presented in this report to evaluate the acoustical transmission loss of the test sample to satisfy building industry requirements in Australia. Each evaluation is made on an analysis of the calculated difference between the filler wall and the filler wall with test sample fitted.

- a. The Internationally used rating of Sound Transmission Class as required by Australian Standard AS1191-2002.
- b. The Weighted Sound Reduction Index, Rw rating with spectral corrections C and Ctr as discussed in International Standards Organisation document ISO717-1:1996 "*Acoustics - Rating of sound insulation in buildings and of building elements - Part 1: Airborne Sound Insulation*". The ISO Rw rating is relevant where the spectra has low frequency energy content and is similar in application to the American OITC criteria. They differ however in the frequency range of application. Each compares a standardised reference curve with the measured data over one-third octave bands. The Rw evaluation is carried out using the one-third octave band with centre frequencies ranging from 100Hz to 3150Hz, and the OITC evaluation is carried out using the one-third octave bands in the frequency range 80Hz to 4000Hz. The Rw criteria is now largely favoured as a replacement for STC. The OITC evaluation is included in our reports for clients who wish to market their products overseas.
- c. Other ratings presented are an evaluation of linear and A-weighted sound transmission loss averaged over the frequency range 100Hz to 5kHz. These are often required for marketing in New Zealand.

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## 7.0 Sound Transmission Class (STC) rating

The first criterion presented, Sound Transmission Class (STC), has been an internationally standardised criterion for many years for evaluating noise reducing characteristics of building elements. The test procedure provides a single number which has been considered sufficient to determine transmission loss of building elements such as walls, windows, doors and other small test samples fitted into the walls of buildings.

This STC rating criterion was originally developed for acoustical performance evaluation of internal walls and doors in buildings and is based on noise spectra with an energy distribution typical of music and speech. It is now considered to be unsuitable for use where the building element under evaluation is likely to be exposed to low frequency components of noise generated by transportation movement.

Determination of Sound Transmission Class for a test sample requires comparison of the measured sound transmission loss with the value for each transmission class rating listed in the STC tables for each one-third octave band centre frequency, 125Hz to 4000Hz. The STC value, which is expressed as a class rating only (not as deciBels) as determined by these tables, is reached when either or both of the following requirements are met:

- (a) The test sample transmission loss at any frequency in the range 125Hz to 4000Hz must not lie more than 8dB below that of the STC reference graph value at the same frequency and
- (b) The total sum obtained from the addition of unfavourable deficiencies (as defined in the “Rw determination” description), must not add to more than 32dB.

## 8.0 Outdoor - Indoor Transmission Class (OITC), and Rw (C; Ctr) Weighted Sound Reduction Ratings

Alternative single number criterion, the American Outdoor - Indoor Transmission Class (OITC) rating and the European International Organisation for Standardisation Document ISO 717-1:1996, specification for the Weighted Sound Reduction Index (Rw) associated with relevant spectrum corrections C and Ctr, have been developed in order to more closely rank transmission loss performance of building elements with a listener’s subjective reaction to transportation and living activity type noise spectra. Each criterion is intended for use in situations where the relevant spectra can be transmitted through the element.

The OITC and Rw (C; Ctr) criterion are not considered to be suitable for use where the noise has a predominantly low frequency component such as produced by some industrial activities. More information on the OITC test procedure can be obtained in ASTM Standard Test Procedure E1332, “*Standard Classification for Determination of Outdoor-Indoor Transmission Class*” and the Weighted Sound Reduction Index, C and Ctr criteria are fully explained in ISO 717-1:1996, “*Acoustics - Rating of sound insulation in buildings and of building elements - Part 1: Airborne Sound Insulation*”.

### 8.1 OITC determination

The OITC value for a test sample, as detailed in ASTM E 1332, is obtained by A-Weighting a noise spectrum which was obtained as an average of multiple measurements of aircraft take-off, freeway and railroad passby activities. This standardised noise spectrum is assumed to be in the send room during measurement of transmission loss.

The noise energy from this assumed noise spectra is (theoretically) transmitted through the small test sample, reduced by the transmission loss of the test sample at each one-third octave centre frequency (each transmission loss obtained from the STC measurement) and then summed as the total energy in the receive room.

The total energy is then determined as sound power (decibel re 1 pW) and the resulting numerical value expressed as the OITC value of the sample under test. It should be noted that the OITC rating is considered as a class evaluation and stated numerically in a similar way to the STC value which is also a class evaluation (that is, stated numerically and not as deciBels as is sometimes found in literature).

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**8.2 Rw determination**

The Rw criterion is obtained by comparing the set of test sample transmission loss against a set of reference data specified on table 3 on page 4 of ISO 717-1: 1996 (the comparison is made between values specified for each set at each one-third octave band centre frequency over the frequency range 100Hz to 3150Hz).

The reference data must then be amplitude shifted by the same amount (in single deciBel steps) until the sum of unfavourable readings, determined from the data difference at each frequency, is as large as possible but not more than 32dB. The 500Hz value of the reference data minus the number of deciBels the reference data set has been shifted is then referred to as the Rw value for the test sample.

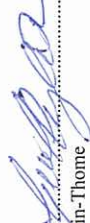
Note 1. An unfavourable difference (deficiency) at any frequency occurs when the test sample transmission loss is less than the value specified for the shifted reference data at the same frequency.

Note 2. The STC rating determination criterion has failure modes of -8dB at any one frequency and/or a deficiency sum of -32dB, whereas Rw has only a single failure mode, this being a -32dB deficiency summation over the pass band consisting of 100Hz to 3150Hz one-third octave bands. As a result of this, the Rw rating usually has the same numerical value as the STC rating unless the STC evaluation is a consequence of one or more -8dB deficiencies and any deficiency at 100Hz does not contribute to the Rw failure or at 4kHz to the STC failure.

**8.3 C and Ctr determination**

Rw corrections are accommodated in ISO 717-1:1996 to account for the type of spectra incident on the high noise side of a test sample. The correction C is applied to Rw spectra which is generated by sources such as transportation which are located close to the building element under test. Such noise sources have a wide energy distribution in their noise spectra. The correction Ctr is applied to pink noise or to spectra which is generated by sources such as transportation, located at a distance. This correction is applied to Rw where spectral energy is mostly concentrated in the low frequency end of the measurement frequency range.

Relevant Spectrum "correction" for different types of noise source (table A.1 of ISO717-1:1996)	
Type of Noise Source	Relevant Spectrum "Correction" Term
Living activities (talking, music, radio, TV) Children playing	C
Railway traffic at medium and high speed Highway road traffic > 80km/hour Jet aircraft, short distance	
Factories emitting mainly medium and high frequency noise Urban road traffic	Ctr
Railway traffic at low speeds Aircraft, propeller driven Jet aircraft, large distance Disco music	
Factories emitting mainly low and medium frequency noise	

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## 9.0 Test environment

Transmission loss measurement according to the requirements of AS1191 requires the use of two reverberation rooms which conform to the acoustical performance requirements of Annex D, guidelines for the design of reverberation rooms, ISO 3741-1999 "Acoustics - Determination of sound power levels of noise sources - Precision methods for broad-band sources in reverberation rooms".

Each test room, designated Reverberation (send) Room and Diffuse Field (receive) Room has a volume of approximately 200 cubic metres and is individually air conditioned by a special purpose acoustically attenuated air conditioning system. During testing, the supply and return air ducts are closed off via both pneumatically and manually operated dampers. The floors have different dimensions and are pentagonally shaped. The ceilings are inclined to the plane of the floor, opposite wall surfaces are different dimensions and inclined at an angle to each other to avoid acoustical coupling between rooms and to minimise the possibility of resonance in each room.

Additional sound diffusion within each of the rooms, to meet diffusivity requirements of ISO 354 - 1985 "Acoustics - Measurement of sound absorption in a reverberation room" is achieved by non-parallel room surfaces together with careful placing of eight 2400mm x 1200mm randomly oriented, freely suspended panels (19mm thick plywood sheets) with a total surface area of 40 square metres. These surfaces are heavily coated with epoxy resin to minimise acoustical absorption. The panels in each room are suspended in accordance with the tuning detail of ISO 354-1985 and therefore fully comply with the requirements of Australian Standard AS1045-1988.

Acoustical absorption coefficients in each octave band for each room and its diffusers do not exceed the maximum AS1191 requirement of 0.06 and are as follows:

Acoustical Absorption Coefficients						
Frequency	125Hz	250Hz	500Hz	1000Hz	2000Hz	4000Hz
Reverberation Room	0.02	0.01	0.02	0.03	0.04	0.06
Diffuse Field Room	0.02	0.02	0.02	0.03	0.04	0.06

Both reverberation rooms are inside separate isolating rooms, which serve as plenum chambers. This construction ensures freedom from flanking noise transmission problems even when very high acoustical sound pressure levels are generated inside either reverberation room.

The 300mm thick walls, floor and ceiling of all three rooms and plenum chambers are made from a heavily reinforced, high density concrete. The reverberation rooms are vibrationally suspended on damped, high tensile springs resting on neoprene rubber. The entire suspension assembly forms a two pole resonant suspension system, which is tuned below 5Hz.

The complete mounting system of springs, dampers and high compliance acoustical seals around the test aperture ensures negligible vibrational coupling between the reverberation rooms or interference from outside vibrational sources for all frequencies within the operating range of the two reverberation rooms. Entry to both reverberation rooms and plenum chambers is by means of double doors.

Each room size, geometry and suspended diffusers ensures that the acoustical performance characteristics fully meet requirements of Australian Standard AS1191-2002.

A sample testing space of approximately 10 square metres is located within an opening in the common wall between the plenum chambers. This wall is part of the external sound shell construction, it is not a component of either test room and effectively isolates the sample from any vibrational energy, which may be generated inside either reverberation test room.

Exposure of either side of any test sample in this test space to a sound field is achieved via apertures in each reverberation room wall which align with the opening in the common wall of the plenum chambers. Acoustical sealing at the location of the openings between the reverberation rooms and the wall holding the test sample is achieved by means of compliant, high transmission loss and vibration isolation gaskets installed between the reverberation rooms and the common wall between the plenum chambers.

When testing small samples a filler wall is constructed in the 10 square metre opening in the testing space. An aperture is made in the filler wall, the test sample is then fitted and sealed in the opening. The acoustical integrity of the fitting is then tested.

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**10.0 Formulae**

**(A) Receive room acoustical absorption**

Sound absorption coefficients at each frequency band for the test specimen alpha (A) is determined from the reverberation time measurements according to the following equation:

$$A = \frac{0.16V}{T_{60}} \dots\dots(1)$$

Where

- A = the equivalent absorption area in the receiving room
- V = the receive room volume (in m<sup>3</sup>)
- T<sub>60</sub> = the receive room reverberation time (RT60)

**(B) Average sound pressure level**

Average sound pressure level (L<sub>p</sub>) is determined for each frequency band as follows:

$$L_p = 10 \text{ Log} \left[ \frac{P_1^2 + P_2^2 + P_3^2 \dots\dots\dots + P_n^2}{n p_o^2} \right] \dots\dots\dots(2)$$

Where

- L<sub>p</sub> = Average sound pressure level (dB)
- P<sub>n</sub> = sound pressure of the n<sup>th</sup> measurement (Pascals)
- P<sub>o</sub> = reference sound pressure (Pascals)
- n = number of measurements

**(C) Transmission Loss**

Since the sound fields in both rooms are diffuse and the environment is free of flanking transmission, sound transmission loss (R) of a test sample for each frequency band is calculated according to the following equation:

$$R = L_{ps} - L_{pr} + 10 \text{ Log} \left[ \frac{S}{A} \right] \dots\dots\dots(3)$$

Where

- R = the sound transmission loss of the test sample
- L<sub>ps</sub> = the average SPL in the source room
- L<sub>pr</sub> = the average SPL in the receiving room
- S = the area of the specimen under test
- A = the equivalent absorption area in the receiving room

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**(D) Small Test Samples**

Test objects comprising a small size test sample mounted in a filler wall are measured according to the small sample method discussed in standard AS1191-2002. The equations used to calculate results are as follows:

Transmission loss coefficients for the small test sample ( $\tau_s$ ) are determined from the difference between the filler wall transmission loss ( $\tau_f$ ) and the composite wall transmission loss ( $\tau_c$ ) according to the following equations:

$$\tau_f = 10^{10 \frac{R_f}{S_f}} \dots\dots\dots(4)$$

$$\tau_c = 10^{10 \frac{R_c}{S_c}} \dots\dots\dots(5)$$

Rearranging the equations produces the transmission loss coefficient for each frequency band as follows:

$$\tau_s = \frac{\tau_c S_c - \tau_f S_f}{S_s} \dots\dots\dots(6)$$

Transmission loss for each frequency band ( $R_s$ ) is determined from this result according to the following equation:

$$R_s = 10 \text{Log} \left[ \frac{1}{\tau_s} \right] \dots\dots\dots(7)$$

Where

- $\tau_c$  = the transmission loss coefficient of the filler wall and the small test sample
- $\tau_f$  = the transmission loss coefficient of the filler wall
- $\tau_s$  = the transmission loss coefficient of the small test sample for each frequency band
- $R_c$  = the transmission loss of the filler wall and the small test sample
- $R_f$  = the transmission loss of the filler wall
- $R_s$  = the transmission loss of the small test sample for each frequency band
- $S_c$  = the surface area of the composite wall
- $S_f$  = the surface area of the filler wall
- $S_s$  = the surface area of the wall mounted small test sample

**(E) Errors**

Errors (95% confidence level) are determined for each frequency band by means of the following equation:

$$\text{Error (95\%confidence)} = \frac{t.sd}{\sqrt{n}} \dots\dots\dots(8)$$

Where

- n = the number of microphone positions sampled
- t = the students t factor
- sd = the standard deviation obtained from the measurement spreadsheet

**11.0 Instrumentation**

The following instrumentation is used for acoustical transmission loss measurements. Instrumentation calibration where appropriate has been calibrated according to NATA requirements.

- Brüel and Kjaer Two Channel Pulse Analyser (assembly 2825, 7521, 2 x 3015), S/N 2005502
- Brüel and Kjaer Real Time Frequency Analyser type 2123, S/N 1446593
- Brüel and Kjaer Cathode Follower type 2639, S/N 1448239 & S/N 1391974
- Brüel and Kjaer Cathode Follower type 2660, S/N 1337994 & S/N 1338051
- Brüel and Kjaer Cathode Follower type 2669, S/N 1888716 & S/N 1834203
- Brüel and Kjaer Microphone type 4144, S/N 563123, S/N 1138528, S/N 439142 & S/N 2118354
- Brüel and Kjaer Microphone type 4179, S/N 2245299, S/N 2245300 & S/N 2245154
- Brüel and Kjaer Sound Level Calibrator type 4231, S/N 2095393
- Yamaha Professional Sound Sources type S500, S/N 1068 and S/N 1069
- Murray 100 Watt Amplifier type MA534, S/N 15
- Vaisala Digital Barometer type PTB201AD, S/N R3330001
- Testo Temperature/Humidity Logger, type 177-H1, S/N 00886924

Leeleed : 

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 Geoff Colfitt-Thome

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Date: 21/9/05.....

Date Of Test  
29-Aug-2008

Signatory  
*Geoff Colvin-Thorne*

Geoff Colvin-Thorne

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Date: 28.1.2005  
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**Test Conditions:**

Total Area Under Test (Sq m): 9.97  
Temperature (C): 18.1  
Relative Humidity SR (%): 64.5  
Relative Humidity RR (%): 64.5  
Barometric Air Pressure (hPa): 1017  
Speed of Sound (m/s): 341.98  
Room Volume (Cu m): 200  
Room Reverb Time (seconds): 3.41

Testing Officer: P. Alway.

**FILLER WALL ONLY**

**ATF Report**

1730

Client Name: Rehan

Frequency	Mean SEND Room SPL (dB) <sub>Sid Dev</sub>	Mean RECEIVE Room SPL (dB) <sub>Sid Dev</sub>	Difference Room Reverb	RT <sub>60</sub> (seconds)	Absorption	10*log (S/A) <sub>Sid Dev</sub>	Calculated 1/3 Octave Transmission Loss (dB)	Precision 95% Interval (dB)	Frequency	Calculated 1/1 Octave Transmission Loss (dB)
50 Hz	90.88	52.25	38.63	6.12	2.80	0.61	41.431	2.43	63 Hz	40.192
63 Hz	89.65	56.25	33.40	4.18	0.85	0.86	34.243	3.66	125 Hz	60.603
80 Hz	90.73	42.47	48.26	1.52	-0.28	0.46	47.980	1.43	250 Hz	70.210
100 Hz	94.58	39.35	55.23	1.69	0.24	0.42	56.470	1.62	500 Hz	80.596
125 Hz	95.12	33.15	61.98	1.48	0.59	0.33	62.561	1.48	1000 Hz	88.288
160 Hz	92.77	31.27	61.50	1.53	2.36	0.40	63.857	1.18	2000 Hz	84.983
200 Hz	94.63	31.35	63.28	0.66	2.55	0.22	65.823	0.87	4000 Hz	92.203
250 Hz	94.38	24.02	70.36	0.77	4.88	0.25	73.467	0.87	8000 Hz	92.237
315 Hz	94.39	20.78	73.62	0.53	3.10	0.25	76.985	0.44		
400 Hz	95.38	20.39	74.99	0.64	3.34	0.16	78.325	0.48		
500 Hz	94.93	16.71	78.22	0.84	3.55	0.12	81.772	0.56		
630 Hz	93.55	12.57	80.98	0.92	3.05	0.09	84.033	0.61		
800 Hz	92.30	9.68	82.62	1.65	2.68	0.08	85.296	1.07		
1000 Hz	94.49	9.53	84.96	0.40	2.46	0.13	87.419	0.33		
1250 Hz	96.71	8.46	87.86	0.29	2.19	0.02	90.050	0.32		
1600 Hz	97.96	9.88	87.56	0.35	1.34	0.07	88.901	0.30		
2000 Hz	95.98	14.59	80.54	0.30	0.75	0.10	81.301	0.39		
2500 Hz	94.69	12.63	80.73	0.35	0.18	0.15	80.907	0.32		
3150 Hz	93.39	4.05	87.10	0.24	-0.35	0.05	86.749	0.31		
4000 Hz	93.38	-2.92	92.91	0.16	-1.08	0.00	91.827	0.41		
5000 Hz	92.45	-4.61	92.41	0.18	-1.90	0.08	90.509	0.60		
6300 Hz	90.20	-6.92	90.62	0.22	-2.78	0.08	87.837	0.70		
8000 Hz	89.76	-6.63	89.18	0.08	-3.76	0.24	85.417	0.54		
10000 Hz	81.69	-5.96	82.83	0.20	-3.89	0.29	78.937	0.54		

**Results (Incorporating AS1191:1985 Compliant Measurements)**

Frequency	Octave Transmission Loss to STC (dB)	STC 82 Curve Loss to STC Difference
50	41	48
63	34	55
80	34	63
100	41	64
125	48	66
150	55	69
200	63	72
250	66	73
315	77	75
400	78	77
500	81	78
630	82	81
800	83	84
1000	85	85
1250	85	85
1500	85	85
2000	86	85
2500	86	85
3150	87	86
4000	92	86
5000	91	85
6300	88	-
8000	85	-
10000	79	-
Sum	91	-30

**The Sound Transmission Class Of This Sample is:**  
STC 82

**The Outdoor Indoor Transmission Class is:**  
OITC 66

Frequency	Normalized A-Weighted Reference Noise Spectrum (dB)	Sound Energy (W/m2)
80 Hz	-19.6	1.738E-07
100 Hz	-17.2	6.026E-08
125 Hz	-15.2	1.514E-08
150 Hz	-15.5	1.122E-08
200 Hz	-14	1.000E-08
250 Hz	-13.7	2.138E-09
315 Hz	-12.7	1.072E-09
400 Hz	-11.9	1.023E-09
500 Hz	-10.3	5.888E-10
630 Hz	-11	3.162E-10
800 Hz	-10.9	2.570E-10
1000 Hz	-11.1	1.549E-10
1250 Hz	-10.5	8.913E-11
1500 Hz	-11.1	9.772E-11
2000 Hz	-10.9	6.457E-10
2500 Hz	-11.8	5.248E-10
3150 Hz	-13.9	8.128E-11
4000 Hz	-15.1	2.774E-07
Sum	-15.1	2.774E-07

**OITC Rating**  
81 (-2; -8)  
81 (-2; -8; -11; -25)

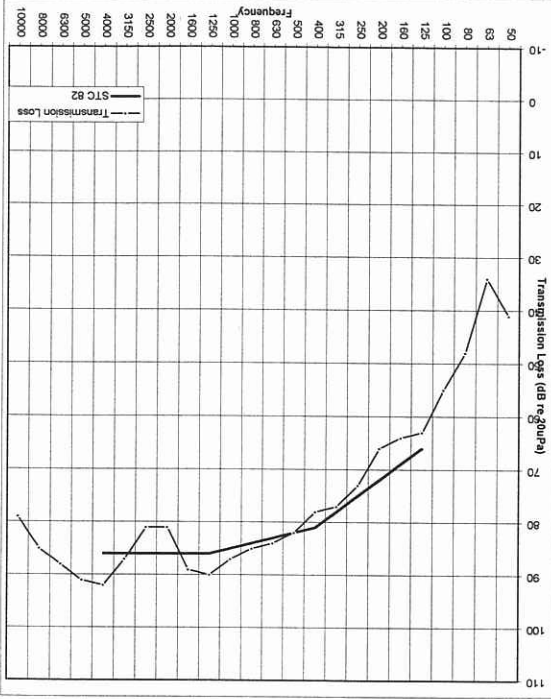
**1/1 Octave**

Frequency	Transmission Loss (dB)	Weighted Reference Noise Spectrum (dB)	Sound Energy (W/m2)
63 Hz	40	-19.6	1.738E-07
125 Hz	61	-17.2	6.026E-08
250 Hz	70	-15.2	1.514E-08
500 Hz	81	-15.5	1.122E-08
1000 Hz	88	-14	1.000E-08
2000 Hz	85	-13.7	2.138E-09
4000 Hz	92	-12.7	1.072E-09
8000 Hz	92	-11.9	1.023E-09

**R<sub>w</sub> Rating**  
81

**CT (50-5000) = -11**  
**CT<sub>R</sub> (50-5000) = -25**

**R<sub>w</sub> Rating**  
81



**Material Under Test:**  
Description: Filler Wall For ATF Test Program August 2005

**Arithmetic Average of Transmission Loss From 100hz to 5kHz**

Frequency	Transmission Loss (dB)	Weighted Average
63 Hz	40	79
125 Hz	61	79
250 Hz	70	75
500 Hz	81	75
1000 Hz	88	75
2000 Hz	85	75
4000 Hz	92	75
8000 Hz	92	75

Date: 31-Aug-2005

Signature: *Geoff Collin-Thorne*

Date Of Test  
31-Aug-2005

Test Conditions:

Total Area Under Test (Sq m): 9.95  
 Temperature (C): 18.3  
 Relative Humidity SR (%): 67.7  
 Relative Humidity RFR (%): 67.7  
 Speed of Sound (m/s): 341.98

Barometric Air Pressure (hPa) 1005  
 Temperature (C) 18.3  
 Relative Humidity SR (%) 67.7  
 Relative Humidity RFR (%) 67.7

Testing Officer: G. Collin-Thorne

FILLER WALL + SAMPLE

ATF Report 1733  
 Client Name: Rehan

Frequency	Mean SEND SPL (dB)	Mean RECEIVE Room SPL (dB)	Difference with Mic Response Corrections	Mean Receive Room Reverb RT60 (seconds)	Absorption 10*log (SA)	STC 47 Loss to STC Difference
50 Hz	86.52	2.70	48.84	2.89	3.72	-3.3
63 Hz	84.36	3.64	47.30	3.35	2.82	-3.3
80 Hz	85.96	2.35	52.40	2.81	2.98	-3.3
100 Hz	87.62	1.63	59.47	3.32	2.63	-3.3
125 Hz	88.30	1.81	62.17	2.57	2.07	-3.3
160 Hz	88.23	1.18	55.12	1.28	1.33	-3.3
200 Hz	89.21	1.17	54.72	1.17	1.18	-3.3
250 Hz	88.38	0.70	53.79	0.78	0.68	-3.3
315 Hz	88.50	0.46	48.55	0.44	0.41	-3.3
400 Hz	88.92	0.50	47.34	0.37	0.39	-3.3
500 Hz	87.87	0.27	46.84	0.56	0.63	-3.3
630 Hz	86.45	0.42	43.49	0.34	0.54	-3.3
800 Hz	86.73	0.28	41.81	0.35	0.44	-3.3
1000 Hz	88.73	0.42	42.63	0.31	0.24	-3.3
1250 Hz	90.76	0.27	45.35	0.24	0.23	-3.3
1600 Hz	91.85	0.24	46.63	0.37	0.28	-3.3
2000 Hz	90.13	0.33	43.54	0.29	0.33	-3.3
2500 Hz	88.59	0.39	38.12	0.33	0.22	-3.3
3150 Hz	86.72	0.34	31.49	0.30	0.20	-3.3
4000 Hz	86.65	0.55	23.37	0.44	0.26	-3.3
5000 Hz	86.48	0.47	16.01	0.32	0.21	-3.3
6300 Hz	83.02	0.78	7.33	0.54	0.15	-3.3
8000 Hz	81.73	1.14	2.27	0.87	0.14	-3.3
10000 Hz	73.63	1.04	-2.32	0.28	0.12	-3.3

Results (Incorporating AS1191-1985 Compliant Measurements)

Rounded 1/3 octave Transmission Loss Values (dB)

Frequency	STC 47 Curve	Loss to STC Difference
50	38	-3
63	36	-3
80	33	-3
100	27	-3
125	28	-3
160	34	-3
200	37	-3
250	38	-3
315	43	-3
400	45	-3
500	46	-3
630	47	-3
800	48	-3
1000	47	-3
1250	48	-3
1600	48	-3
2000	46	-3
2500	49	-3
3150	51	-3
4000	53	-3
5000	59	-3
6300	64	-3
8000	69	-3
10000	67	-3
Sum	-28	-3

The Sound Transmission Class Of This Sample is: **STC 47**

The Outdoor Indoor Transmission Class is: **OITC 39**

Normalized A-Weighted Reference Noise Spectrum (dB)

Frequency	Sound Energy (W/m2)
80 Hz	-19.6
100 Hz	-17.2
125 Hz	-15.2
160 Hz	-15.6
200 Hz	-14
250 Hz	-13.7
315 Hz	-12.7
400 Hz	-11.9
500 Hz	-10.3
630 Hz	-11
800 Hz	-10.9
1000 Hz	-11.1
1250 Hz	-10.5
1600 Hz	-11.1
2000 Hz	-10.9
2500 Hz	-11.8
3150 Hz	-13.9
4000 Hz	-15.1
Sum	1.357E-04

Weighted A-Reference Noise Spectrum (dB)

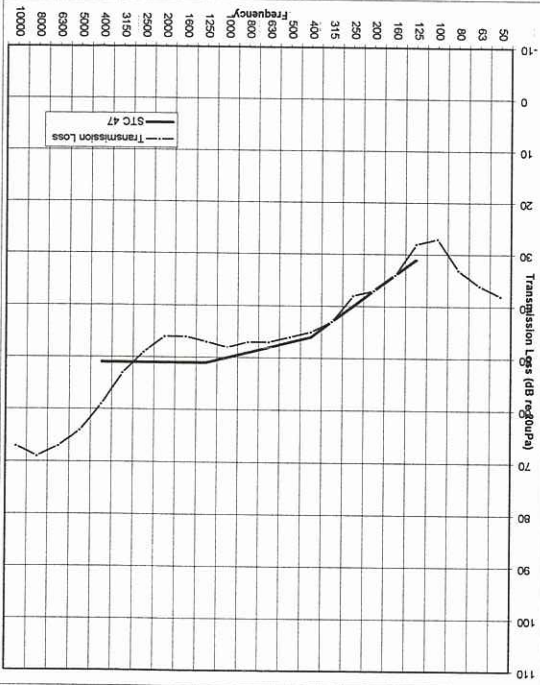
Frequency	Sound Energy (W/m2)
63 Hz	36
125 Hz	39
250 Hz	39
500 Hz	46
1000 Hz	48
2000 Hz	48
4000 Hz	59
8000 Hz	74

1/1 Octave Rounded 1/3 octave Transmission Loss Values (dB)

Frequency	Loss Values (dB)
63 Hz	36
125 Hz	39
250 Hz	39
500 Hz	46
1000 Hz	48
2000 Hz	48
4000 Hz	59
8000 Hz	74

1/1 Octave R<sub>w</sub> Rating

R<sub>w</sub> = 47  
 C<sub>1</sub> = -2  
 C<sub>2</sub> = -5  
 C<sub>TR</sub> = -1  
 C<sub>T</sub> (50-5000) = -6  
 C<sub>TR</sub> (50-5000) = -6



Material Under Test:  
 PVC Casement Window with fixed light.  
 Glazing - Insulating Glass Unit (0.38mm Lam (Send Side)/ 16mm air gap/ 6.76mm Laminated Glass (Receive Side)  
 EPDM Interior and exterior perimeter seals.  
 5mm Self-adhesive foam on interior stile.

Arithmetic Average of Transmission Loss From 100hz to 5Khz

Unweighted Average: 45  
 A-Weighted Average: 40

Calculated 1/3 Octave Transmission Loss (dB)

Frequency	Loss (dB)
63 Hz	36.251
125 Hz	30.373
250 Hz	38.976
500 Hz	45.687
1000 Hz	47.936
2000 Hz	47.800
4000 Hz	58.688
8000 Hz	74.208

**ATF Report 1733**

Client Name: Rehan

**SAMPLE ONLY**

Date Of Test  
31-Aug-2005

**Test Conditions:**

Surface Area Of Test Sample (Sq m): 2.3436  
 Surface Area Of Remaining Filler Wall: 7.6264  
 Total Surface Area Of Test Aperture: 9.97

Signatory: *[Signature]*  
 Geoff Colvin-Thome

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Date: 21.9.05  
 Page 12 of 13

Results (Incorporating AS1191-1985 Compliant Measurements)	
Frequency	Loss Values (dB)
10000 Hz	50
8000 Hz	63
6300 Hz	80
5000 Hz	21
4000 Hz	21
3150 Hz	22
2500 Hz	28
2000 Hz	28
1600 Hz	28
1250 Hz	28
1000 Hz	28
800 Hz	28
630 Hz	28
500 Hz	28
400 Hz	28
315 Hz	28
250 Hz	28
200 Hz	28
160 Hz	28
125 Hz	28
100 Hz	28
80 Hz	28

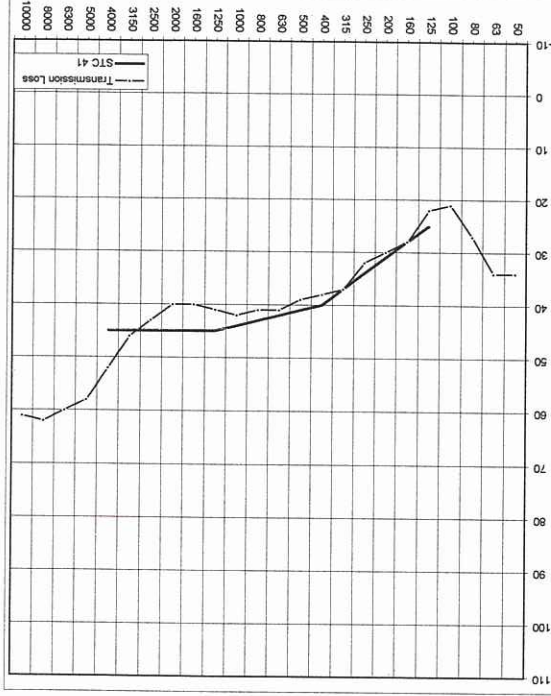
Frequency	Loss (dB)	Transmission Loss	Filler Wall +
10000 Hz	41.43	32.22	7.19253E-05
8000 Hz	44.3	32.24	0.000376449
6300 Hz	47.98	33.23	1.59239E-05
5000 Hz	55.47	27.28	2.8379E-06
4000 Hz	62.56	28.29	5.54451E-07
3150 Hz	65.86	34.48	0.001481859
2500 Hz	68.82	36.56	2.61648E-07
2000 Hz	73.47	36.56	4.50142E-08
1600 Hz	76.98	42.94	2.00228E-08
1250 Hz	78.33	44.56	3.49844E-05
1000 Hz	80.91	49.14	8.11451E-09
800 Hz	81.30	46.41	7.4106E-09
630 Hz	86.90	46.11	1.28791E-09
500 Hz	88.90	47.14	9.86826E-10
400 Hz	90.05	47.14	1.93379E-05
315 Hz	92.42	48.47	1.81196E-09
250 Hz	94.87	48.47	1.81196E-09
200 Hz	97.28	47.26	2.95614E-09
160 Hz	98.03	47.26	1.88061E-05
125 Hz	101.07	47.26	1.87132E-05
100 Hz	103.33	47.26	1.87132E-05
80 Hz	105.33	46.11	1.81196E-05
63 Hz	107.14	46.11	1.81196E-05
50 Hz	108.90	46.11	1.81196E-05

Frequency	Normalized A-Weighted Reference Noise Spectrum (dB)	Sound Energy (W/m2)
80 Hz	-19.6	2.188E-05
100 Hz	-17.2	1.514E-04
125 Hz	-15.2	4.467E-04
160 Hz	-15.5	4.467E-05
200 Hz	-14	3.981E-05
250 Hz	-13.7	2.692E-05
315 Hz	-12.7	1.072E-05
400 Hz	-11.9	1.023E-05
500 Hz	-10.3	1.175E-05
630 Hz	-11	6.310E-06
800 Hz	-10.9	6.457E-06
1000 Hz	-11.1	4.898E-06
1250 Hz	-10.5	7.079E-06
1600 Hz	-11.1	7.762E-06
2000 Hz	-10.9	8.128E-06
2500 Hz	-11.8	3.311E-06
3150 Hz	-13.9	1.203E-06
4000 Hz	-15.1	5.530E-04

Frequency	1/f <sup>2</sup>	Loss (dB)	Transmission Loss	Filler Wall +
50 Hz	243.39	33.998	0.000470799	0.000158031
63 Hz	268.77	34.230	0.000377533	0.000376449
80 Hz	125.73	27.050	0.001972572	1.59239E-05
100 Hz	156.67	22.005	0.005302229	5.54451E-07
125 Hz	158.67	22.005	0.00156419	2.8379E-06
160 Hz	1610.58	28.192	0.000938684	1.59239E-05
200 Hz	1610.58	30.275	0.000208955	2.61648E-07
250 Hz	1610.58	32.070	0.000225822	4.50142E-08
315 Hz	1610.58	36.577	0.000215928	7.99782E-05
400 Hz	1610.58	38.275	0.000148781	1.87132E-05
500 Hz	1610.58	39.309	0.00011724	1.87132E-05
630 Hz	1610.58	40.848	7.99782E-05	1.87132E-05
800 Hz	1610.58	40.848	12156.14	1.81196E-05
1000 Hz	1610.58	42.186	15642.17	1.81196E-05
1250 Hz	1610.58	42.186	12156.14	1.81196E-05
1600 Hz	1610.58	39.817	9588.33	1.81196E-05
2000 Hz	1610.58	40.226	0.000104293	2.28376E-05
2500 Hz	1610.58	42.857	9.71304E-05	2.28376E-05
3150 Hz	1610.58	40.226	10295.44	1.21862E-05
4000 Hz	1610.58	42.857	174087.55	5.74424E-06
5000 Hz	1610.58	46.249	1.69785E-06	3.99770E-07
6300 Hz	1610.58	57.701	588981.54	9.37063E-07
8000 Hz	1610.58	60.282	1067164.27	2.21592E-07
10000 Hz	1610.58	62.448	1757248.58	5.69071E-07

Frequency	1/1 Octave	Loss Values (dB)
63 Hz	32	41
80 Hz	24	41
100 Hz	24	41
125 Hz	33	41
160 Hz	33	41
200 Hz	39	41
250 Hz	33	41
315 Hz	33	41
400 Hz	39	41
500 Hz	33	41
630 Hz	33	41
800 Hz	39	41
1000 Hz	33	41
1250 Hz	33	41
1600 Hz	42	41
2000 Hz	42	41
2500 Hz	42	41
3150 Hz	52	41
4000 Hz	52	41
5000 Hz	68	41

Frequency	Confidence Interval (dB)	Loss (dB)	Transmission Loss
50 Hz	3.51	33.998	0.000470799
63 Hz	4.85	34.230	0.000377533
80 Hz	2.85	27.050	0.001972572
100 Hz	2.77	22.005	0.005302229
125 Hz	2.50	22.005	0.00156419
160 Hz	1.64	28.192	0.000938684
200 Hz	1.18	30.275	0.000208955
250 Hz	0.96	32.070	0.000225822
315 Hz	0.61	36.577	0.000215928
400 Hz	0.63	38.275	0.000148781
500 Hz	0.71	39.309	0.00011724
630 Hz	0.71	40.848	7.99782E-05
800 Hz	1.12	40.848	12156.14
1000 Hz	0.50	42.186	15642.17
1250 Hz	0.40	42.186	12156.14
1600 Hz	0.47	39.817	9588.33
2000 Hz	0.56	40.226	0.000104293
2500 Hz	0.44	42.857	9.71304E-05
3150 Hz	0.64	40.226	10295.44
4000 Hz	0.68	42.857	174087.55
5000 Hz	0.92	57.701	1.69785E-06
6300 Hz	0.68	60.282	1067164.27
8000 Hz	1.26	62.448	1757248.58
10000 Hz	1.35	62.448	1757248.58



Frequency	Unweighted Average	A-Weighted Average
34	38	34

Sample Under Test: PVC Casement Window with fixed light.  
 Glazing - Insulating Glass Unit 10.38mm Lam (Send Side)/ 16mm air gap/  
 6.7mm Laminated Glass (Receive Side)  
 EPDM Interior and exterior perimeter seals.  
 5mm Self-adhesive foam on interior stile.

Calculated 1/3 Octave Transmission Loss (dB)	Frequency	Confidence Interval (dB)
31.566	63 Hz	4.85
24.088	125 Hz	2.50
32.690	250 Hz	0.96
39.400	500 Hz	0.71
41.649	1000 Hz	0.50
41.513	2000 Hz	0.46
52.401	4000 Hz	0.64
67.972	8000 Hz	1.26

Date: *27.7.05*

**R<sub>w</sub> Calculation Spreadsheet**

Frequency (Hz)	Transmission Loss R <sub>i</sub> (Rounded down to 1 significant figure)	Rw 41 Curve	Sum
100	22	22	22
125	22	22	22
150	28	-3	-3
175	28	-	-
200	30.3	-0.7	-0.7
250	32.1	-1.9	-1.9
315	36.7	-0.3	-0.3
400	38.3	-1.7	-1.7
500	39.3	-1.7	-1.7
630	41	-2	-2
800	41	-1.8	-1.8
1000	42.2	-4.2	-4.2
1250	40.8	-4.9	-4.9
1500	39.8	-5.2	-5.2
1600	40.1	-4.9	-4.9
2000	42.9	-2.1	-2.1
2500	46.2	-	-
3150	45	-	-

**Transmission Loss R<sub>i</sub> (Rounded down to 1 significant figure)**

Frequency (Hz)	Transmission Loss R <sub>i</sub> (Rounded down to 1 significant figure)
50	33.9
60	34.2
80	27.0
100	21.0
125	22.0
150	28.2
160	30.3
200	32.1
250	32.1
315	36.7
400	38.3
500	39.3
630	41.0
800	41.0
1000	42.2
1250	40.8
1500	39.8
1600	40.1
2000	42.9
2500	46.2
3150	45.2
4000	52.4
5000	57.7

**Determination Of Correction C**

C spectrum (ISO 717-P7)	L <sub>i</sub> -R <sub>i</sub>	10 <sup>n</sup> ((L <sub>i</sub> -R <sub>i</sub> )/10)	Sum
-29	-50.00	1.000E-05	1.262E-04
-26	-48.00	1.585E-05	38.99
-23	-51.20	7.586E-06	
-21	-51.50	7.413E-06	
-19	-51.10	7.762E-06	
-17	-53.70	4.266E-06	
-15	-53.30	4.677E-06	
-13	-52.30	5.888E-06	
-12	-53.00	5.012E-06	
-11	-52.00	6.310E-06	
-10	-52.20	6.026E-06	
-9	-49.80	1.047E-05	
-9	-48.80	1.318E-05	
-9	-49.10	1.230E-05	
-9	-51.90	6.457E-06	
-9	-55.20	3.020E-06	
-50.00			1.262E-04

**Determination Of Correction C<sub>50-5000</sub>**

C spectrum (ISO 717-P11)	L <sub>i</sub> -R <sub>i</sub>	10 <sup>n</sup> ((L <sub>i</sub> -R <sub>i</sub> )/10)	Sum
-41	-74.90	3.236E-08	
-37	-71.20	7.586E-08	
-34	-61.00	7.943E-07	
-30	-51.00	1.259E-05	
-27	-49.00	1.259E-05	
-24	-52.20	6.026E-06	
-22	-52.30	5.888E-06	
-20	-52.10	6.166E-06	
-18	-54.70	3.388E-06	
-16	-54.30	3.715E-06	
-14	-53.30	4.677E-06	
-13	-54.00	3.981E-06	
-12	-53.00	5.012E-06	
-11	-53.20	4.786E-06	
-10	-50.80	8.318E-06	
-10	-49.80	1.047E-05	
-10	-50.10	9.772E-06	
-10	-52.90	5.129E-06	
-10	-56.20	2.399E-06	
-10	-62.40	5.754E-07	
-10	-67.70	1.698E-07	
1.019E-04			39.92

**Determination Of Correction CTR**

C spectrum (ISO 717-P7)	L <sub>i</sub> -R <sub>i</sub>	10 <sup>n</sup> ((L <sub>i</sub> -R <sub>i</sub> )/10)	Sum
-20	-41.00	7.943E-05	
-20	-42.00	6.310E-05	
-18	-46.20	2.399E-05	
-16	-46.30	2.344E-05	
-15	-47.10	1.950E-05	
-14	-50.70	8.511E-06	
-13	-51.30	7.413E-06	
-12	-51.30	7.413E-06	
-11	-52.00	6.310E-06	
-9	-50.00	1.000E-05	
-8	-50.20	9.550E-06	
-9	-49.80	1.047E-05	
-10	-49.80	1.047E-05	
-10	-51.10	7.762E-06	
-13	-55.90	2.570E-06	
-15	-61.20	7.586E-07	
2.907E-04			35.37

**Determination Of Correction C<sub>TR, 50-5000</sub>**

C spectrum (ISO 717-P11)	L <sub>i</sub> -R <sub>i</sub>	10 <sup>n</sup> ((L <sub>i</sub> -R <sub>i</sub> )/10)	Sum
-25	-58.90	1.288E-06	
-23	-57.20	1.905E-06	
-21	-48.00	1.585E-05	
-20	-41.00	7.943E-05	
-20	-42.00	6.310E-05	
-18	-46.20	2.399E-05	
-16	-46.30	2.344E-05	
-15	-47.10	1.950E-05	
-14	-50.70	8.511E-06	
-13	-51.30	7.413E-06	
-12	-51.30	7.413E-06	
-11	-52.00	6.310E-06	
-9	-50.00	1.000E-05	
-8	-50.20	9.550E-06	
-9	-49.80	1.047E-05	
-10	-49.80	1.047E-05	
-10	-51.10	7.762E-06	
-10	-52.90	5.129E-06	
-10	-56.20	2.399E-06	
-10	-62.40	5.754E-07	
-10	-67.70	1.698E-07	
3.099E-04			35.09

**Determination Of Arithmetic Average Of Transmission Loss**

Frequency (Hz)	Transmission Loss	Calculated	A-weighted	Average =
100	20.995	20.995	19.1	100
125	22.005	22.005	-16.1	125
150	28.192	28.192	-13.4	160
175	30.275	30.275	-10.9	200
200	32.070	32.070	-8.6	250
250	36.657	36.657	-6.6	315
300	38.275	38.275	-4.8	400
315	39.309	39.309	-3.2	500
400	40.970	40.970	-1.9	630
500	40.970	40.970	-1.9	800
630	42.186	42.186	0	1000
800	40.848	40.848	0.6	1250
1000	39.817	39.817	1	1500
1250	42.126	42.126	1.2	2000
1500	42.857	42.857	1.3	2500
1600	46.249	46.249	1.2	3150
2000	52.408	52.408	1	4000
2500	57.701	57.701	0.5	5000

**34.441**  
**34.074**

**A-weighted Transmission Loss**